

New power semiconductor technology for renewable energy sources application

By
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SEMIKRON

Sevilla

Mai 12. 2005

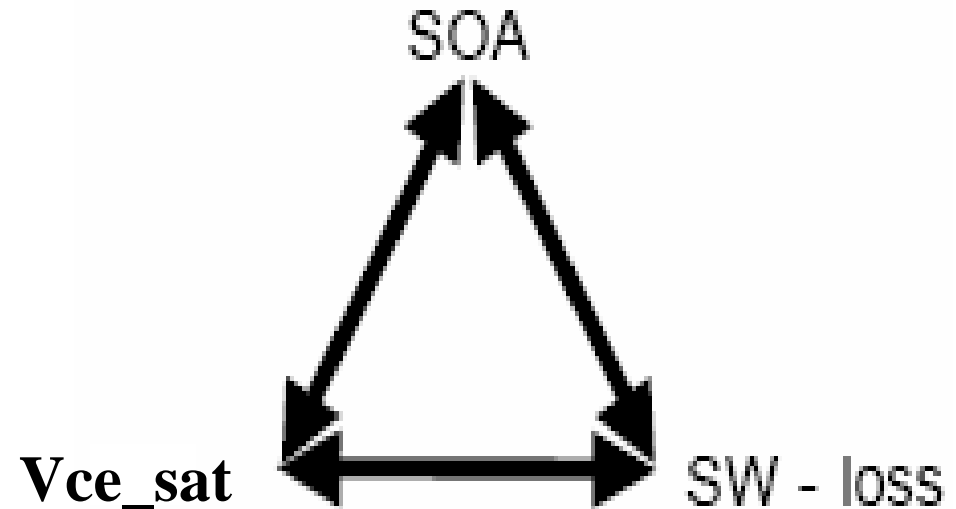


IGBT is the working horse of power electronics

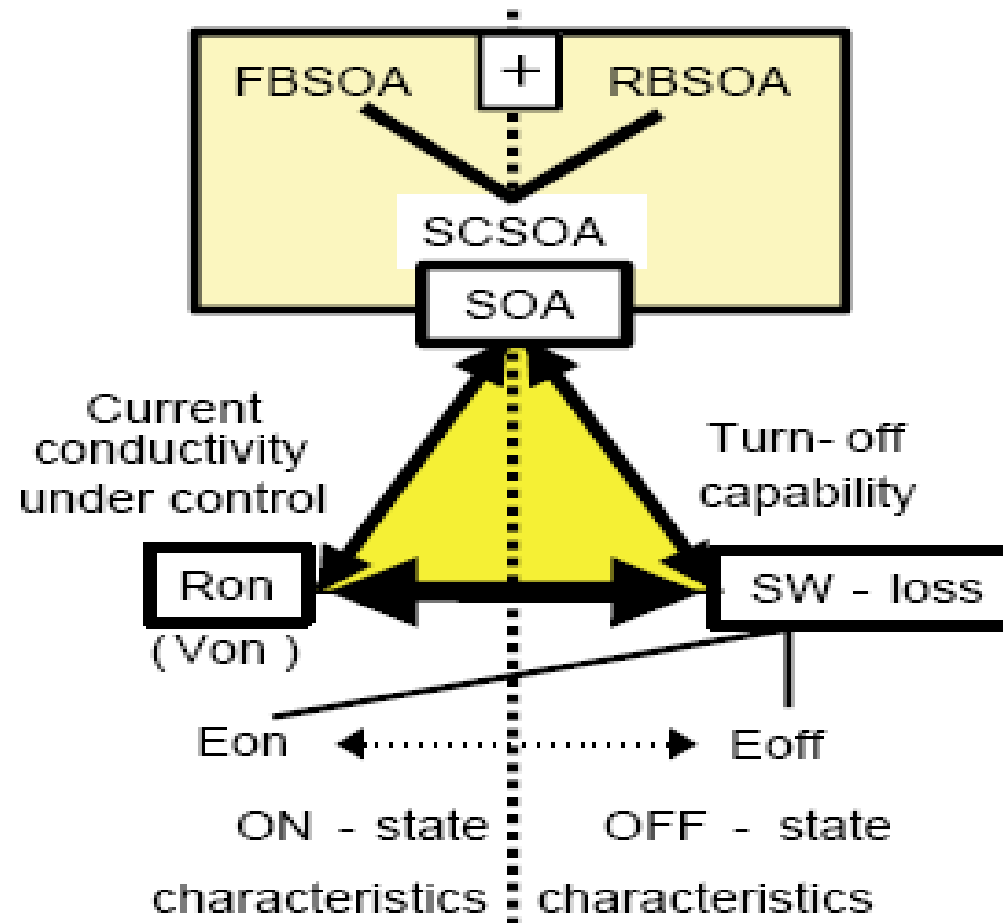
In power semiconductor devices there is a trade-off between the forward current conducting capabilities (the ON resistance and/or the forward voltage drop) and the turn-off capabilities (the forward-blocking capabilities), where advances in these devices are measured in terms of improvements in this trade-off relationship



- FBSOA - RBSOA
- V_{ce_sat}
- SW - loss
- Turn- off capability
- Current conductivity under control
- OFF – state characteristics
- ON – state characteristics
- SCSOA (Short Circuit SOA)



by Tadaharu Minato and Hideki Takahashi Mitsubishi Electric ADVANCE



by Tadaharu Minato and Hideki Takahashi Mitsubishi Electric ADVANCE

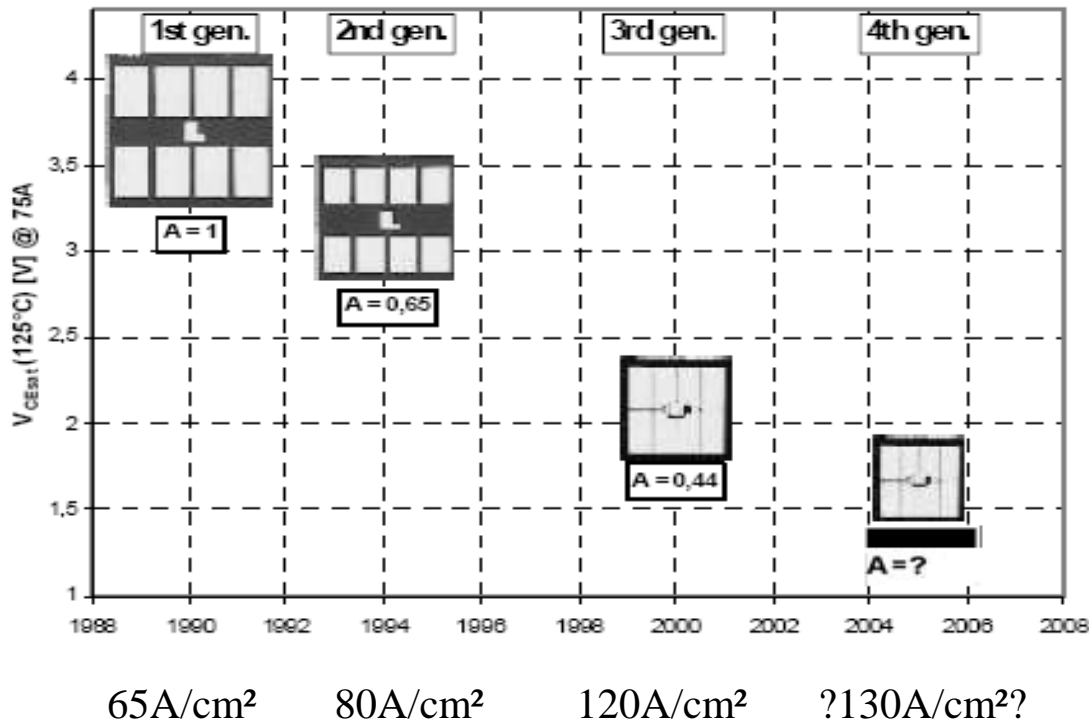
IGBT Parameters



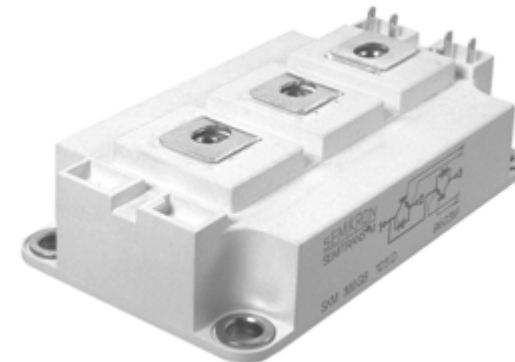
For traditional 600V, 1200V and 1700V applications in the industrial drives segment an essential demand for short circuit capability of IGBTs exists. Among others this is one reason why the robust

“Non Punch Through” IGBT technology with homogeneous base material dominated the original “Punch Through” concept based on Epitaxial technology. In the last several years a tendency towards a new vertical structure, PT type (thin substrate + buffer layer) called “Trench - Field Stop IGBT3” by Infineon and “Soft Punch Through” IGBT (SPT) by ABB or CSTBT by Mitsubishi.

Because of economic reasons there is a strong demand for smaller chips.



1988: SKM200GB120D
 1994: SKM300GB123D
 2000: SKM400GB128D
 2002: SKM600GB126D

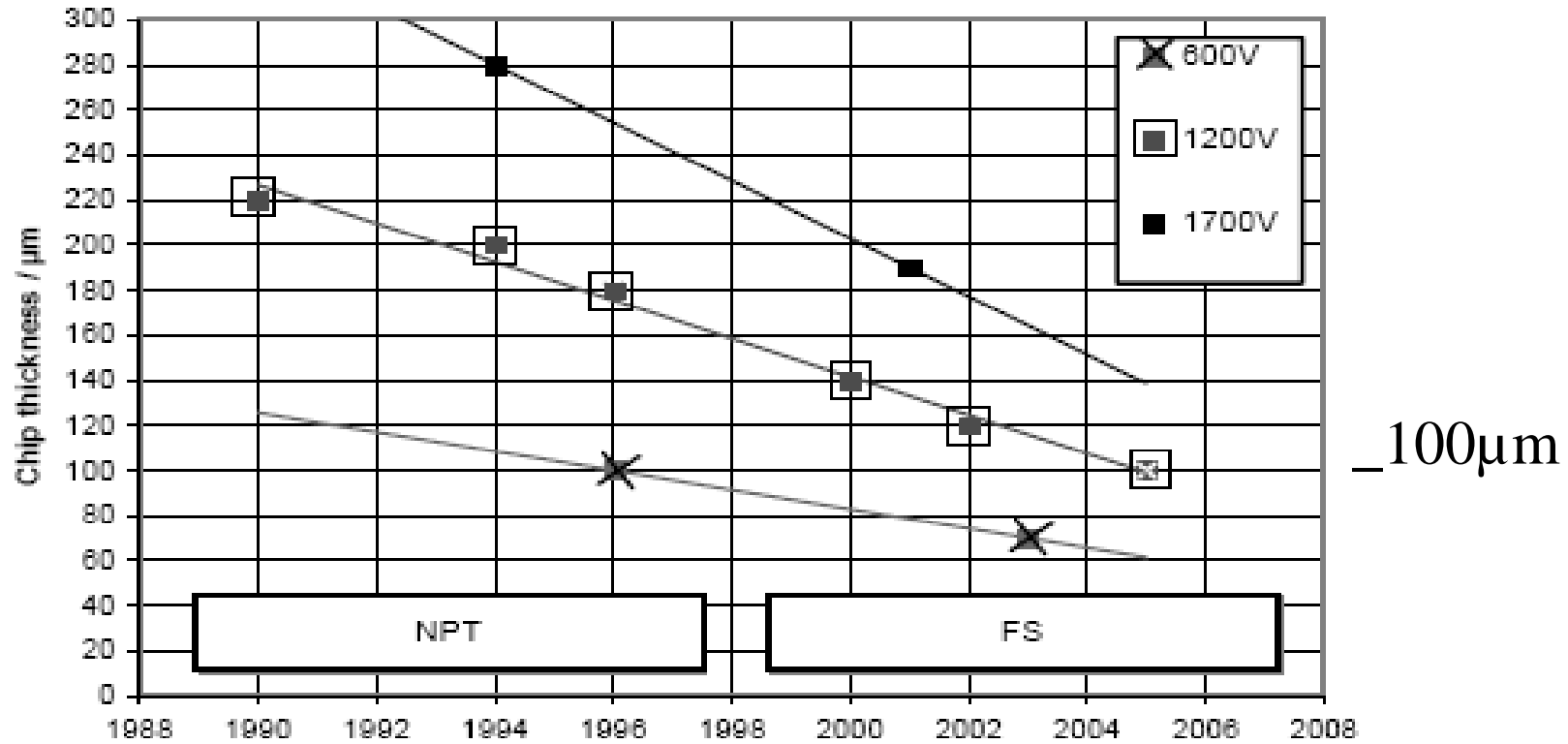


Chip shrink of a 75A/1200V-IGBT Chips

The increase of the IGBT module currents over the last 15 years.

Current density of IGBT Chips

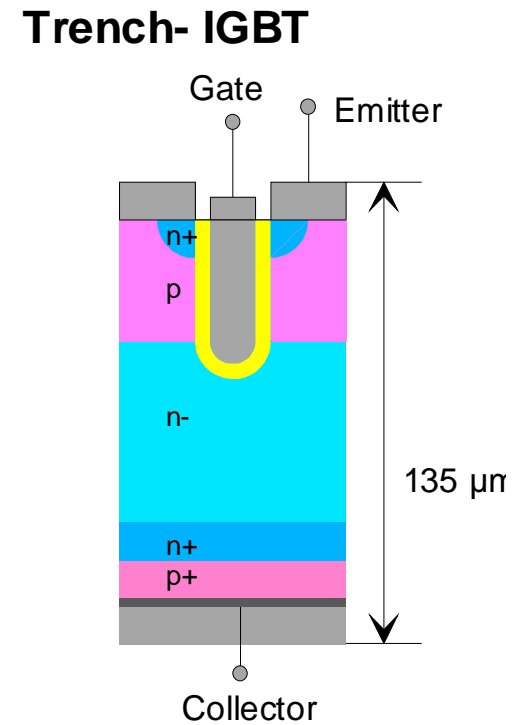
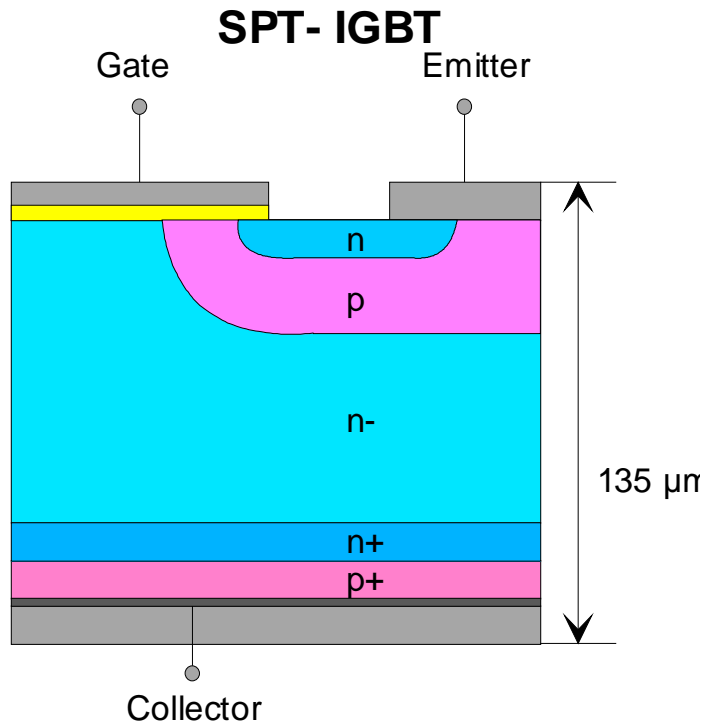




Decrease of chip thickness for NPT and SPT (Field-Stop) IGBTs;
past and forecast

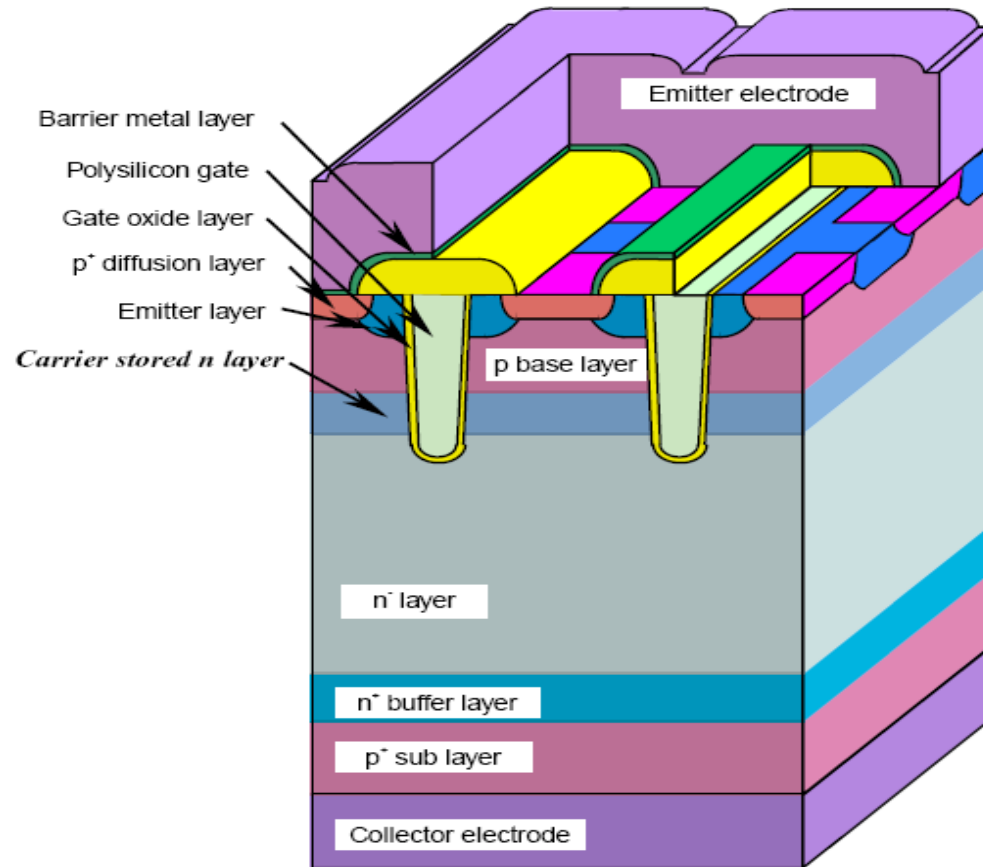
Thickness of IGBT Chips





IGBT Structure: SPT and Trench

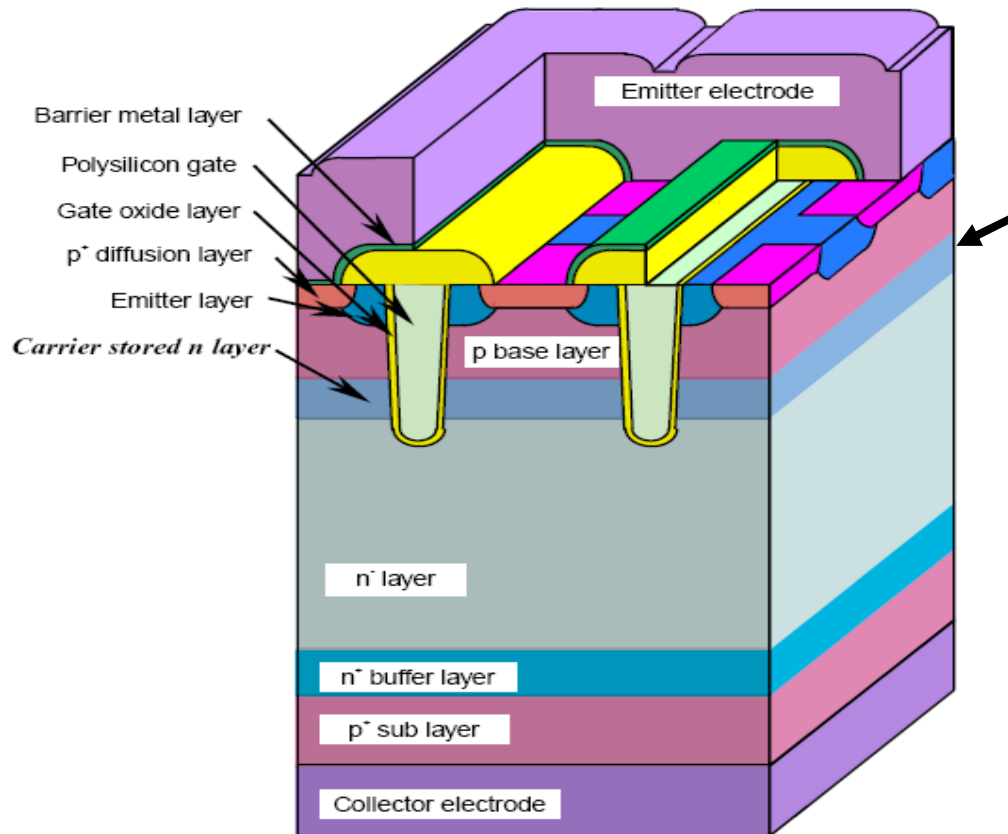




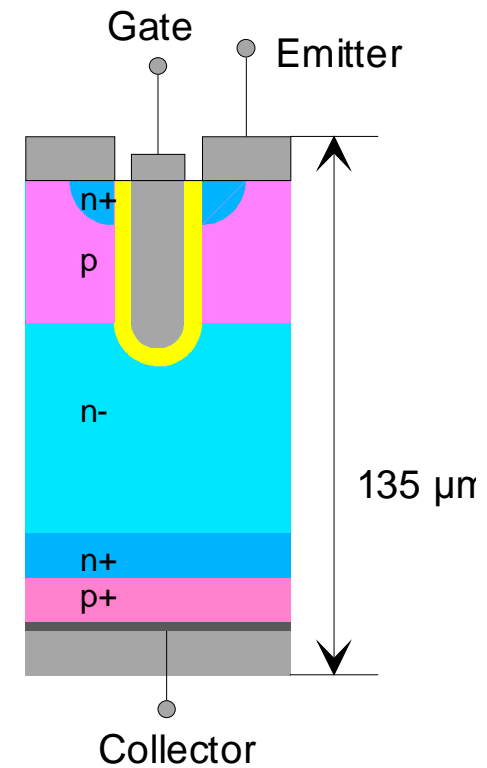
The Carrier-Stored Trench-gate Bipolar Transistor (CSTBT)

The CSTBT structure





Trench- IGBT

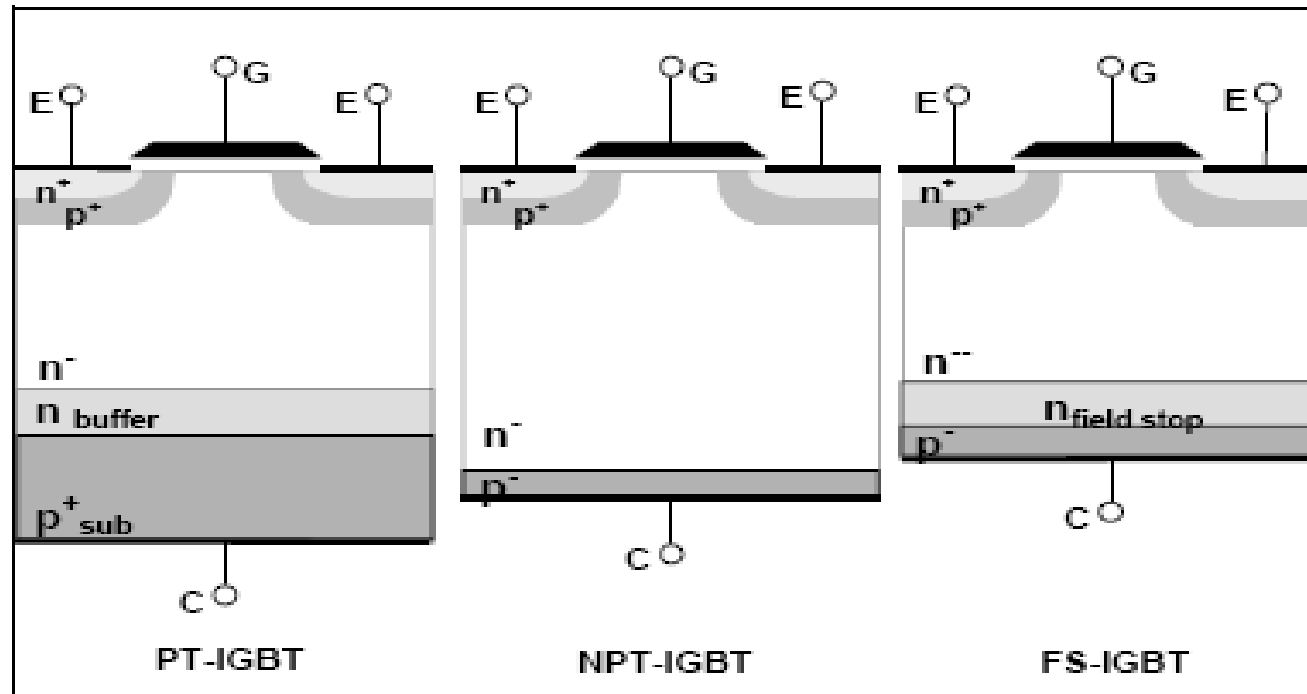


The CSTBT structure



- 1980 IGBT structure patent application
- ('86) **PT-IGBT** 2 layered Epitaxy (n+/n-), planar gate, DMOS (Double Diffused MOS)
- 1988 **NPT-IGBT** n- substrate, thin wafer, planar gate
- (96s) **PT Trench gate**
- ('99s) **Trench Gate field stop IGBT**
- ('00s) **Soft Punch Through, Planar Gate IGBT, SPT**
- ('01s) **PT-CSTBT** (Carrier Stored Trench IGBT)
- ('05s) **SPT + (PLUS), Soft Punch Through, Planar Gate IGBT**, low switching losses, **Ultra Soft**
- (late '90s) NPT-IGBT **RB-IGBT** (Reverse Blocking IGBT)
- ('04s) **LPT-IGBT** (LPT-CSTBT) **RC-IGBT** (Reverse Conducting IGBT)





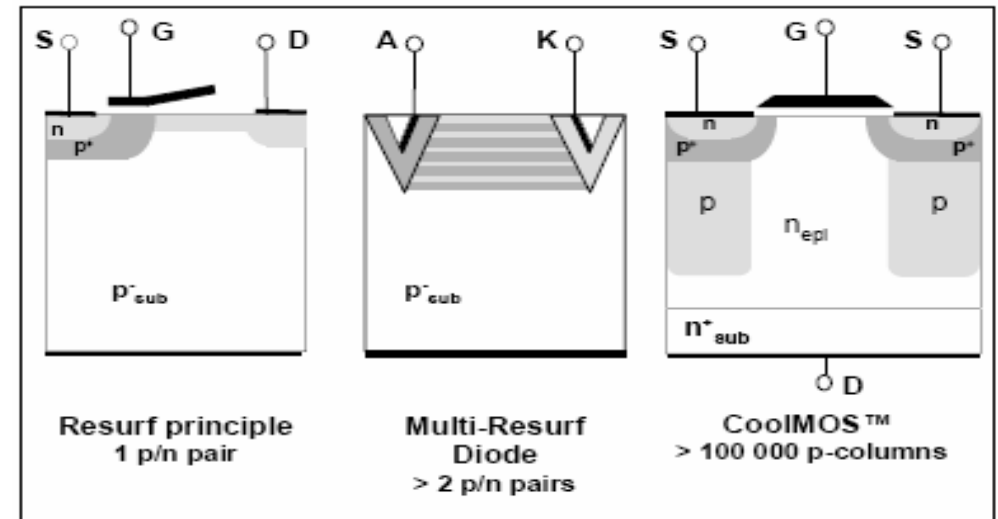
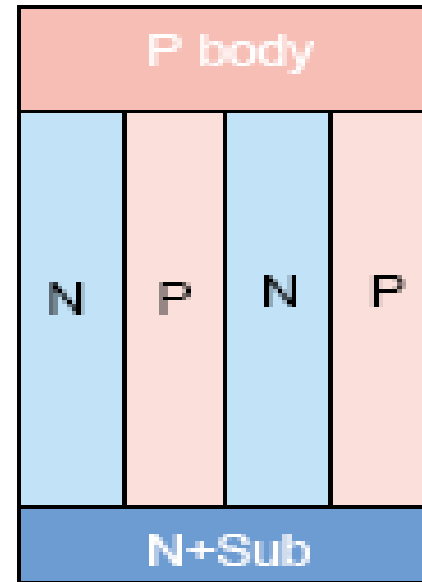
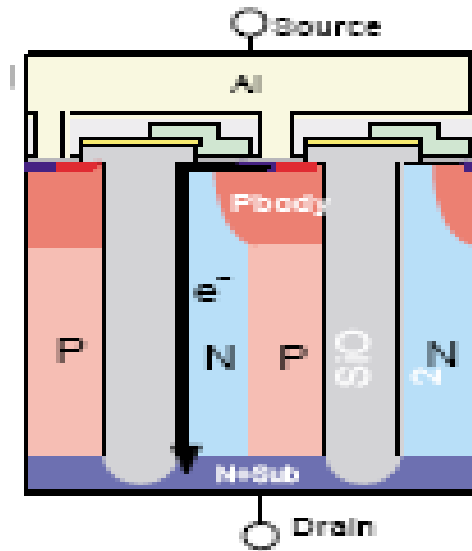
IGBT Chip design



■ --- Future technology ---

- 2007 Self Clamping IGBT; RB-IGBT; RC-IGBT
- 2009 **Super Junction**, for >1200V (Like Cool MOS structure, vertical or planar, extreme low V_{ce_sat})
- 2010 SiC Devices (ex. Junction -FET)
(SBD : Schottky Barrier Diode known today)





Vertical Structure

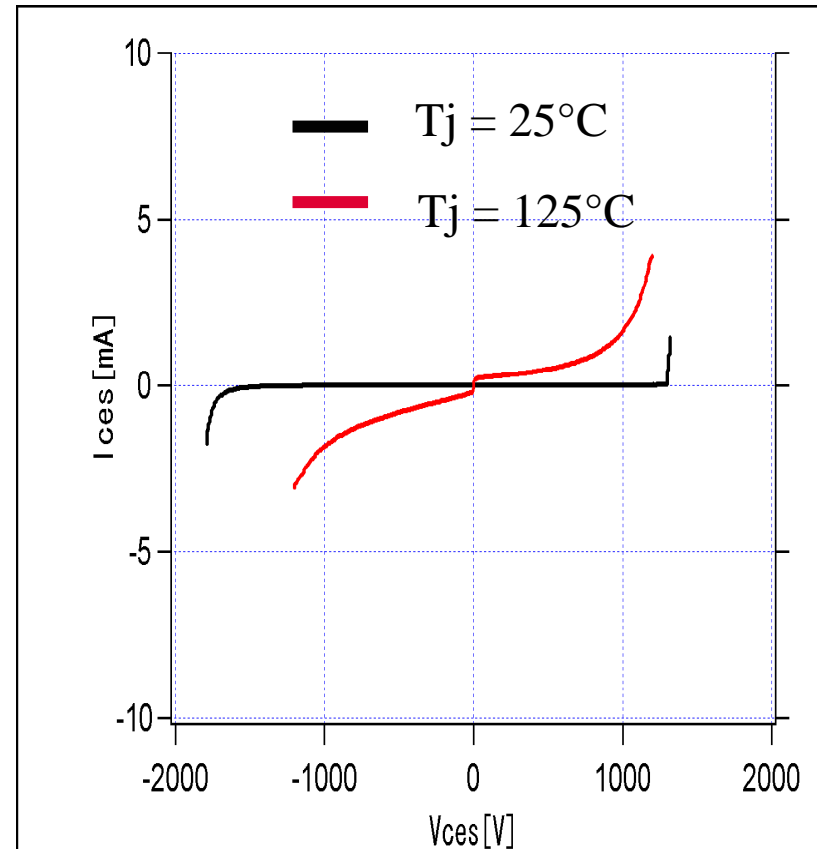
Super Junction Technology



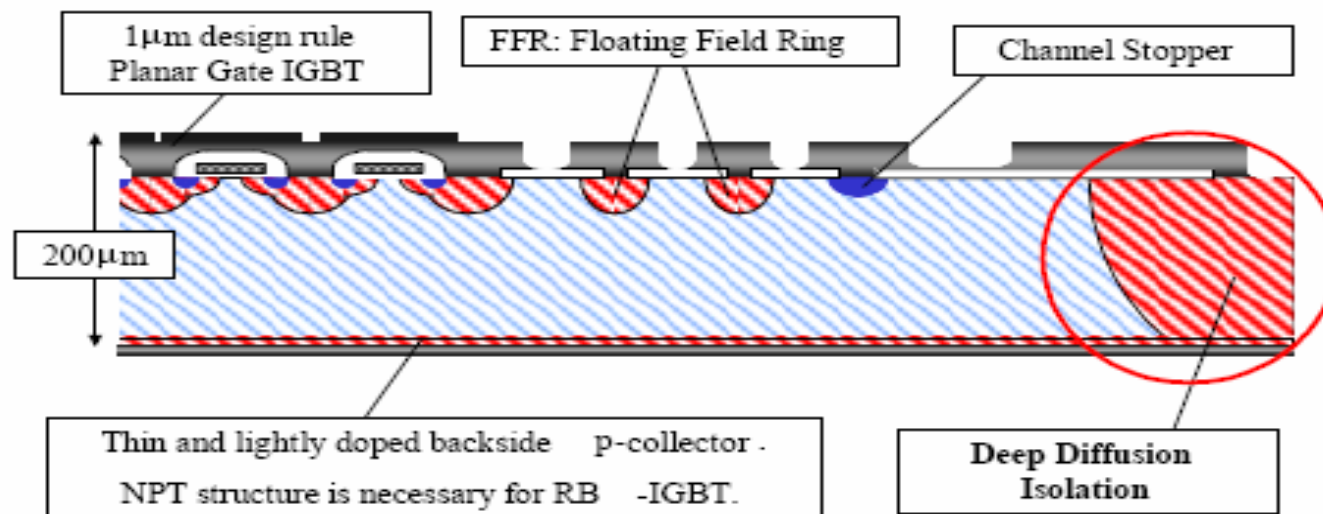
Reverse Blocking IGBT

- The RB-IGBT has a symmetrical blocking voltage characteristic. This means that it can block both forward and reverse voltage in its off state.

As a result the bidirectional switching element can be simplified because the need for series connected diodes is eliminated.

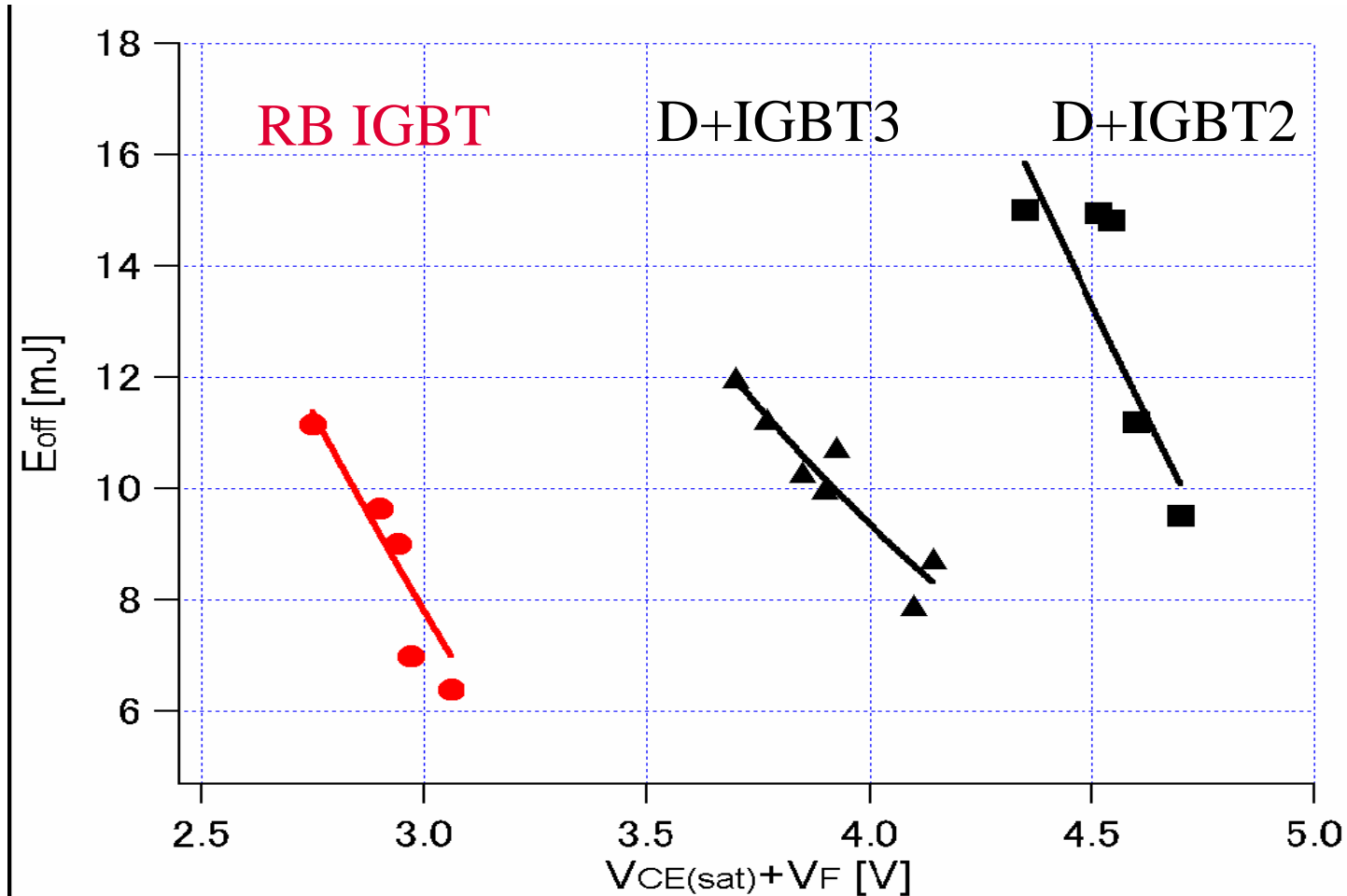


The RB-IGBT is similar to a conventional IGBT except that it has a deep diffusion collector wall surrounding the chip active area. This collector isolation allows the IGBT to block reverse voltage. The isolation is produced using a special process designed to maintain a high breakdown voltage and stable leakage current characteristics at elevated temperatures while minimizing processing time.



RB-IGBT Chip Structure

E_{off} versus On-state voltage drop trade-off



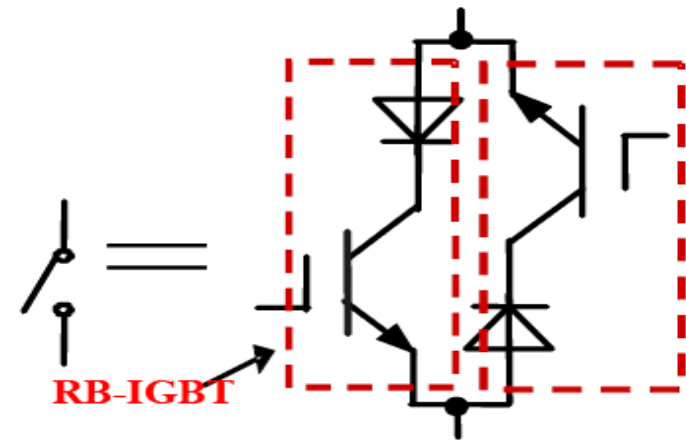
New Semiconductors: RB IGBT



Almost all semiconductor producers are able to produce RB IGBT.
Only, there is no demand for a mass production,
no industrial applications for such a product.

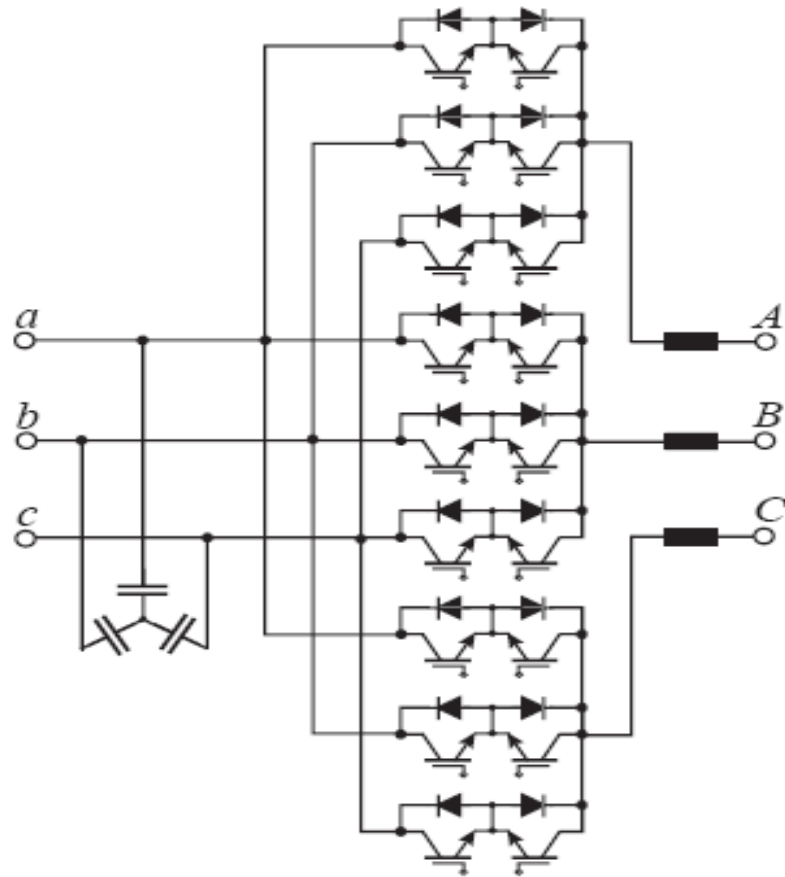
Application demands for RB IGBT:

- Matrix Converter
- Current source inverter
- Static switch
- AC Voltage Control



RB-IGBT Producers and Application fields

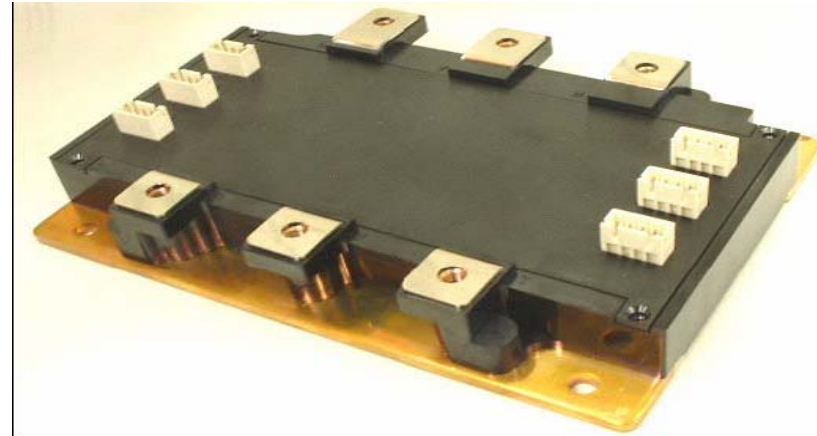
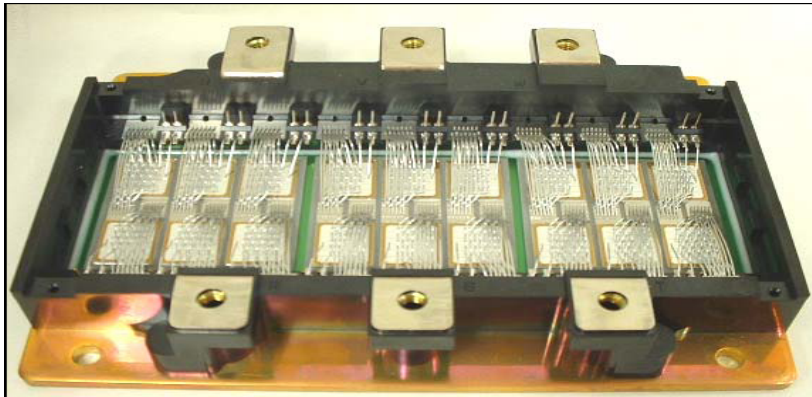




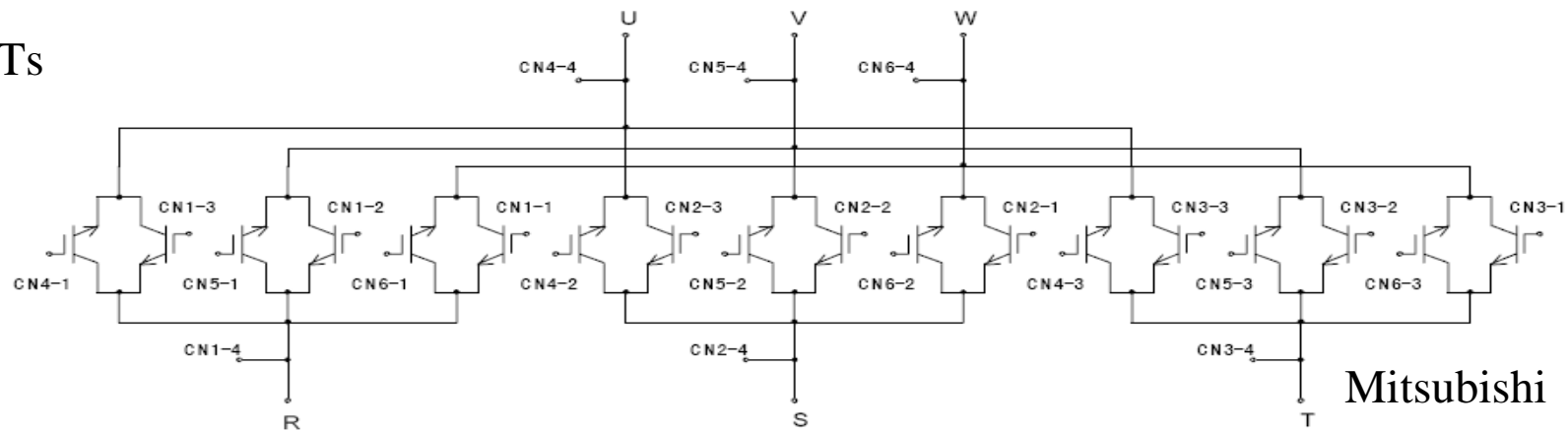
With existing IGBTs and series diodes

Matrix Converter

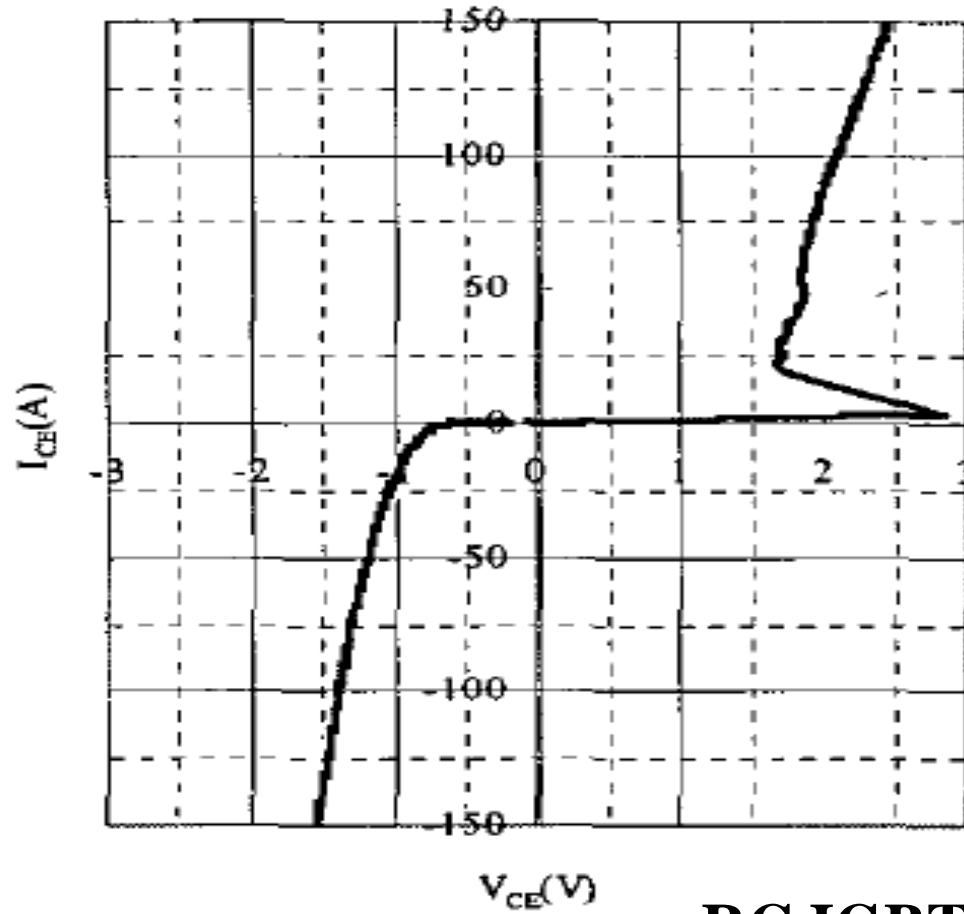




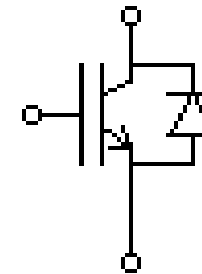
RB IGBTs



Matrix Converter Module Prototype



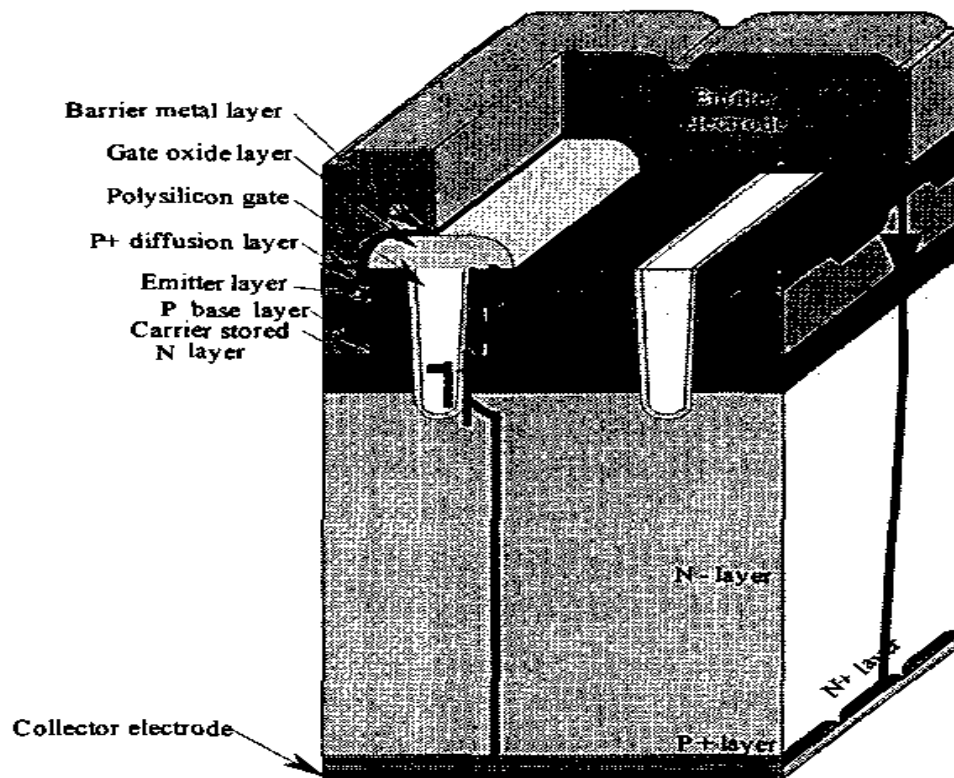
IGBT Chip with built-in FWD



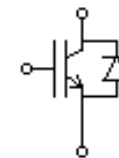
RC IGBT Output Characteristics

Reverse Conducting **IGBT**





The strip N-region and strip P-region are independently formed on the wafer backside in the orthogonal-crossing direction to the wafer front side trench-gate stripe direction, instead of forming conventional stacking N-buffer and P-collector layers. P-region and N-region are formed side by side in the backside structure



IGBT with built-in FWD

Three dimensional view of RC IGBT structure

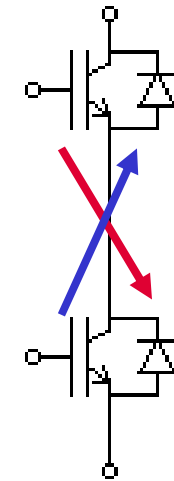


RC IGBT Application: voltage source converters

- + Compact construction of IGBT and its FWD
- + Less bonding wires
- + Relatively simple Chip construction
- + Better chips utilization, lower chip rand, (guard rings) structure
- IGBT and diode losses are on the same chip
- IGBT is near to the own FWD, but there is no force current commutations between those two elements

Top IGBT commutate with bottom diode

and bottom IGBT commutate with top diode



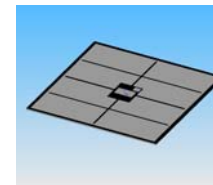
RC IGBT



The term IGBT indicates a unit- cell structure in an area several microns wide on a silicon chip.

The user, on the other hand, thinks of it as a white (or black) plastic package, on the heatsink, and the final product characteristics, I_c , V_{ce_sat} , $E_{on\&E_{off}}$, R_{th_ch} , typically SOA, reliability, durability, etc; are also viewed as expressions of the device rather than the performance of the chip itself.

How to make IGBT chip packaging?



What is an IGBT?

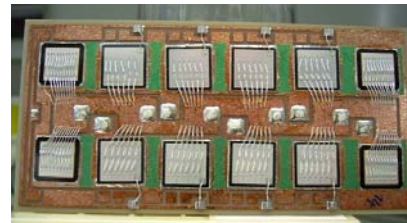
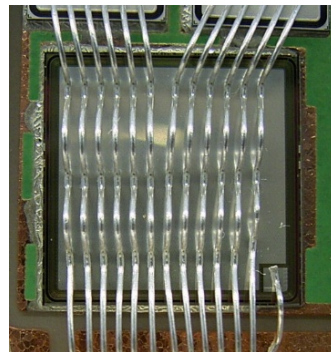
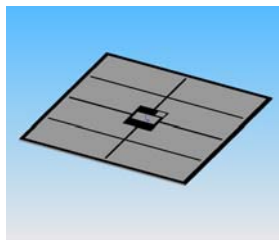
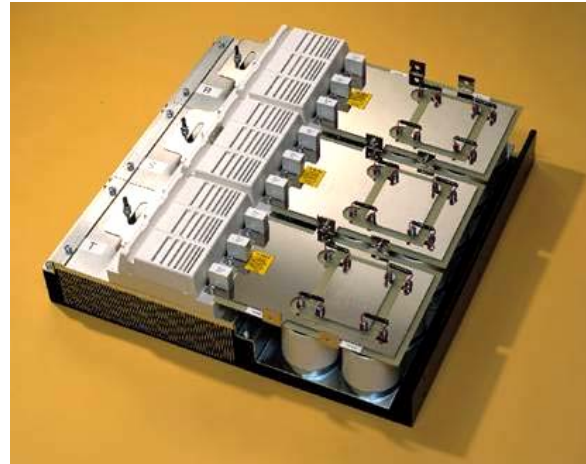
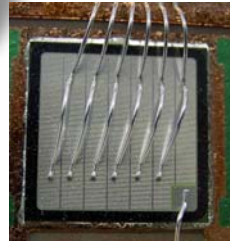


Open questions

- Silicon Chips produce the losses and have to be placed on the heatsink.
- An isolation between chips and heatsink is needed - ceramic substrate DCB
- Construction with low stray inductances
- High power converters needs a lot of chips in parallel; how to parallelized them
- Applied electrical circuit
- High power needs a high current. Higher voltage needs less current. How to make **Medium Voltage** converters
- **MV** silicon
- **MV** windmills
- Wind parks and off-shore applications

From Chips to the Windmills





From the wafers to the Windmills

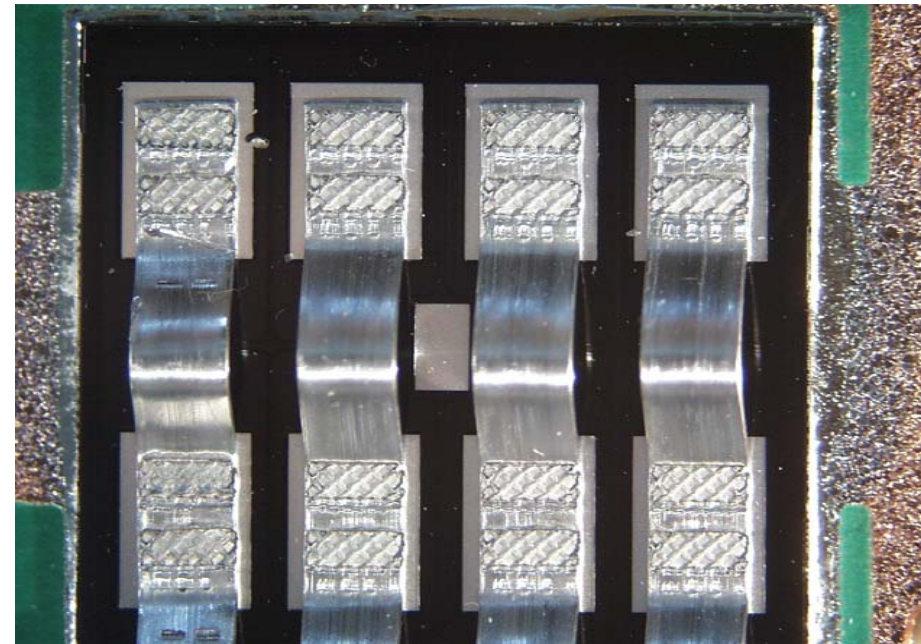


Ribbon Bonds allow 2-4 times higher Current Densities than traditional Bond Wires



300µm

60x8 mil



IGBT with Ribbon Bonds

Ribbon Bonding Technology

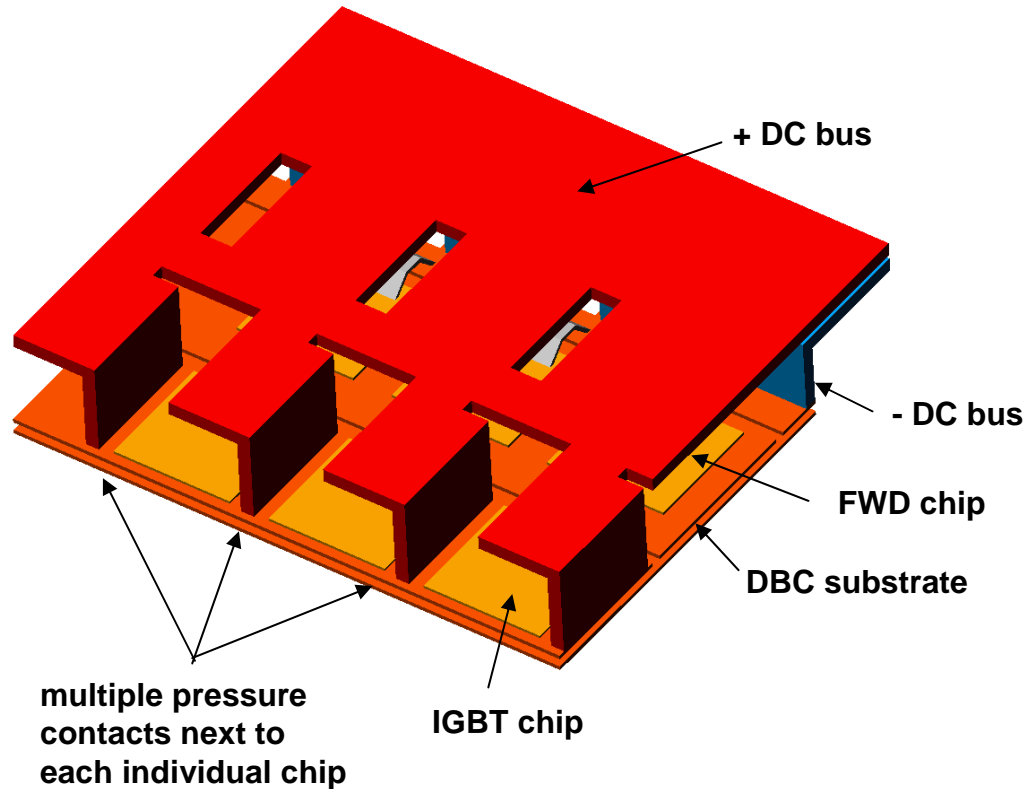


Low inductance is crucial

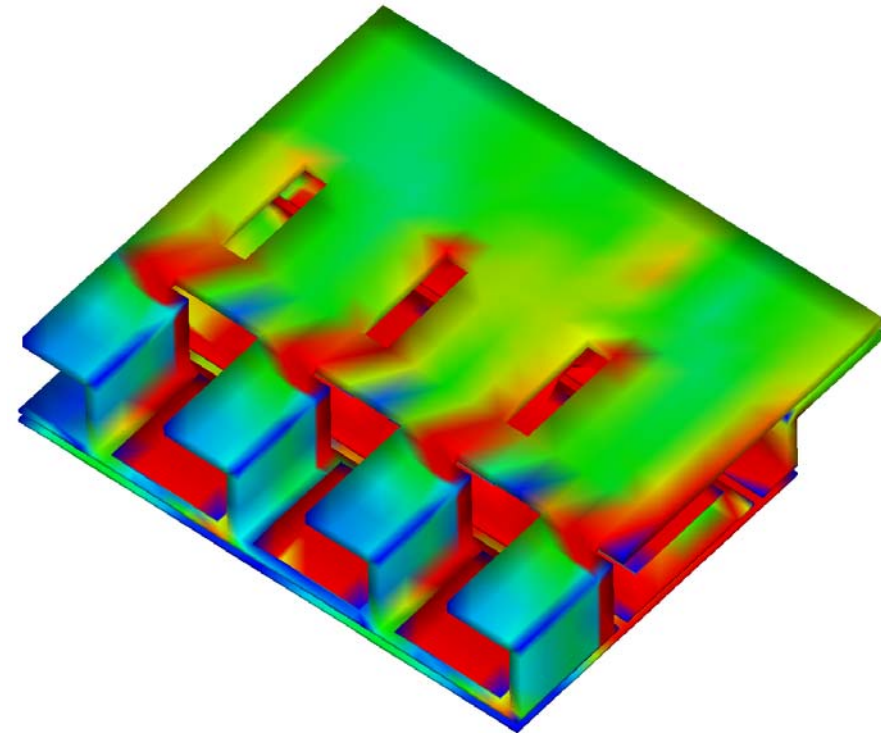
- Every switch cycle is creating overvoltage spikes.
- For fast switching transients the parasitic inductance L_{σ} need to be small $V = L_{\sigma} di/dt$
- Overvoltage spikes are causing EMI problems
- Optimum current sharing of paralleled devices
- No need for additional snubber capacitors

Challenge: Inductance





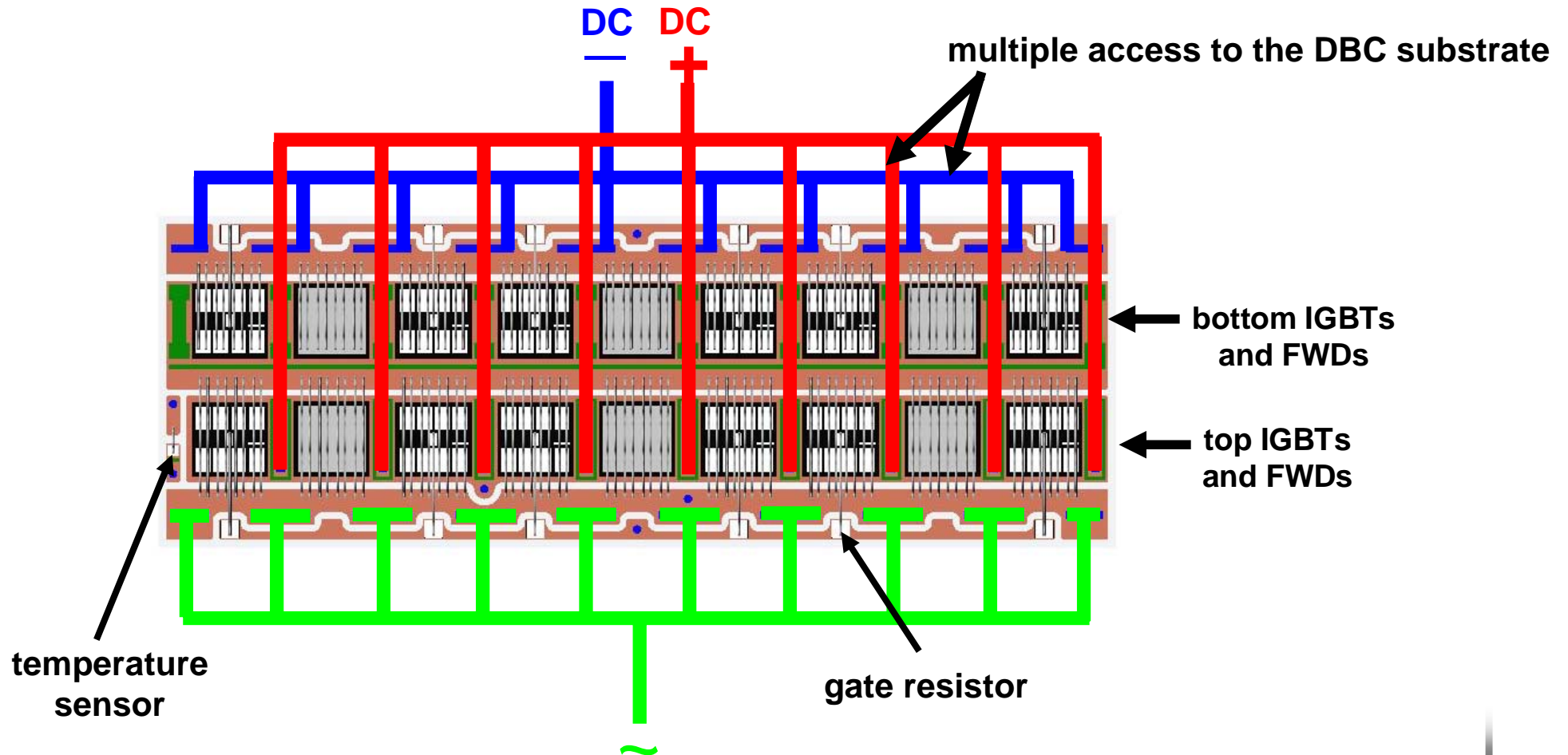
**Simplified model for simulating
DC link and DBC substrate**



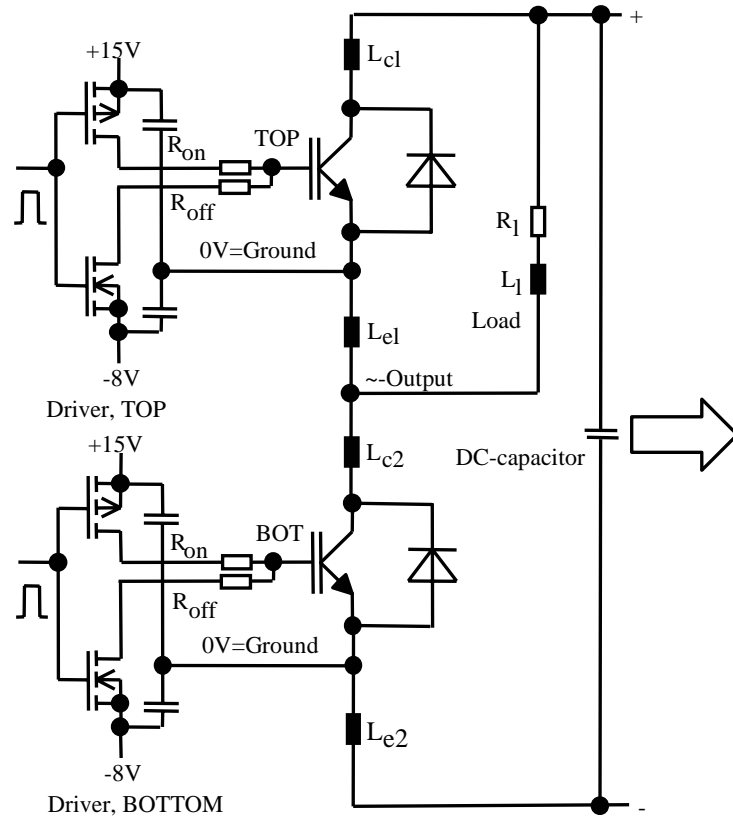
**Simulated current density
(top IGBTs are turned on)**

Simulation of Electromagnetic and Thermal Properties





Low Parasitic Inductance of the Construction



Module

L_{CE}

Semitrans 3

20 nH

SKiiP 2

15 nH

SKiiP 3

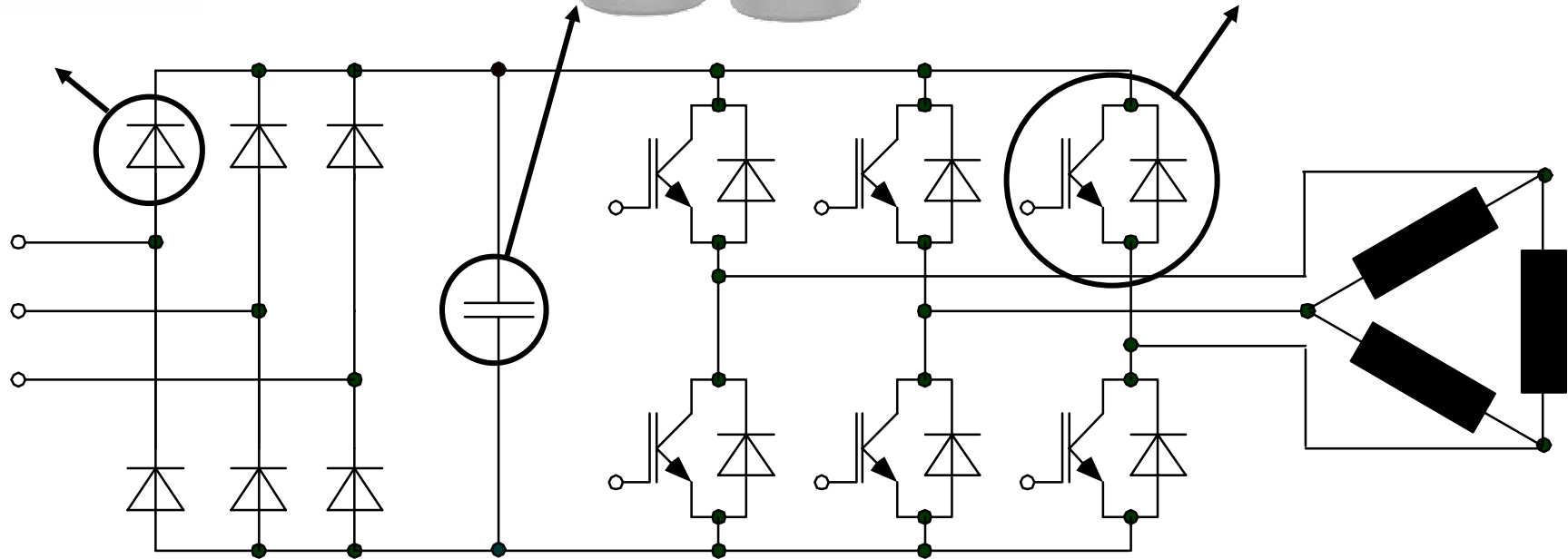
7.5 nH

HV SKAI

4.0 nH

Commutation Inductance L_{CE}

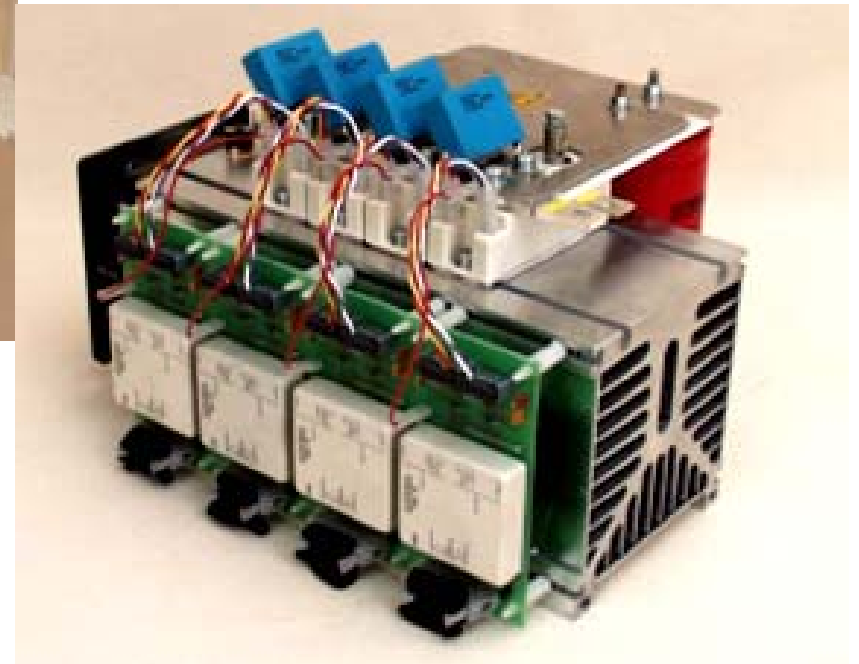




Power Semiconductors, DC Link Capacitors, Cooling, Bus Bars, Sensors, Drivers, Controller, Housing

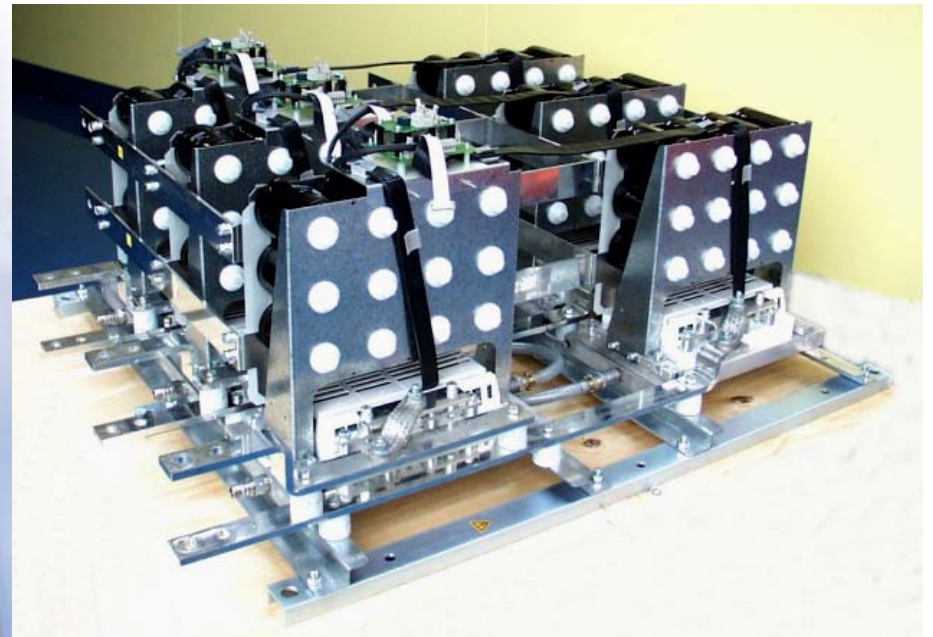
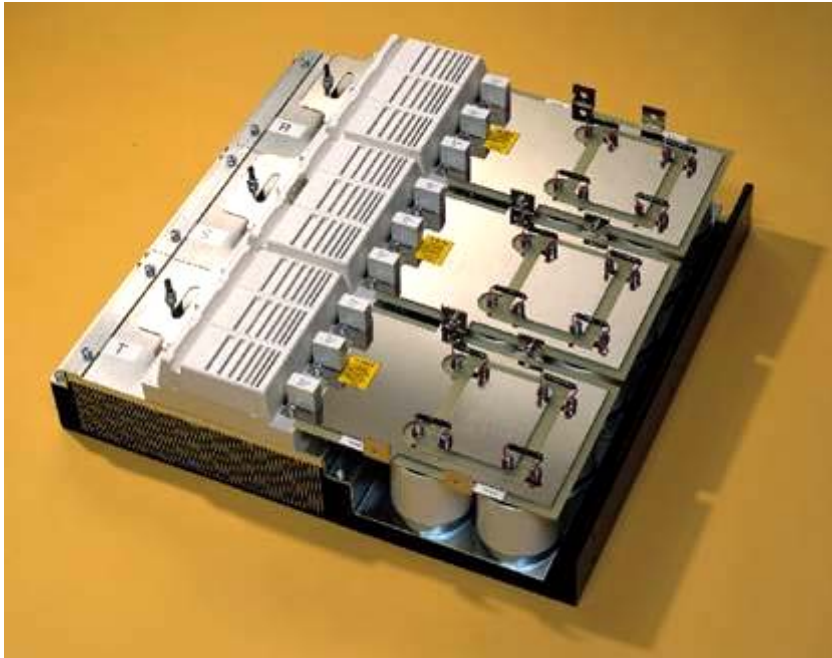
Drives Solution with Discrete Components





Solutions with Discrete Components



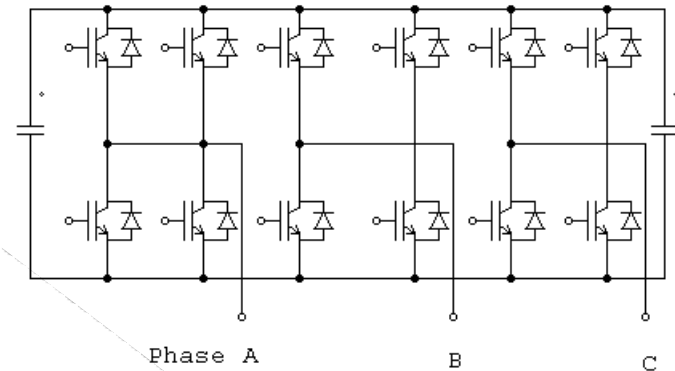


High Power Inverters in SKiiP-Technology

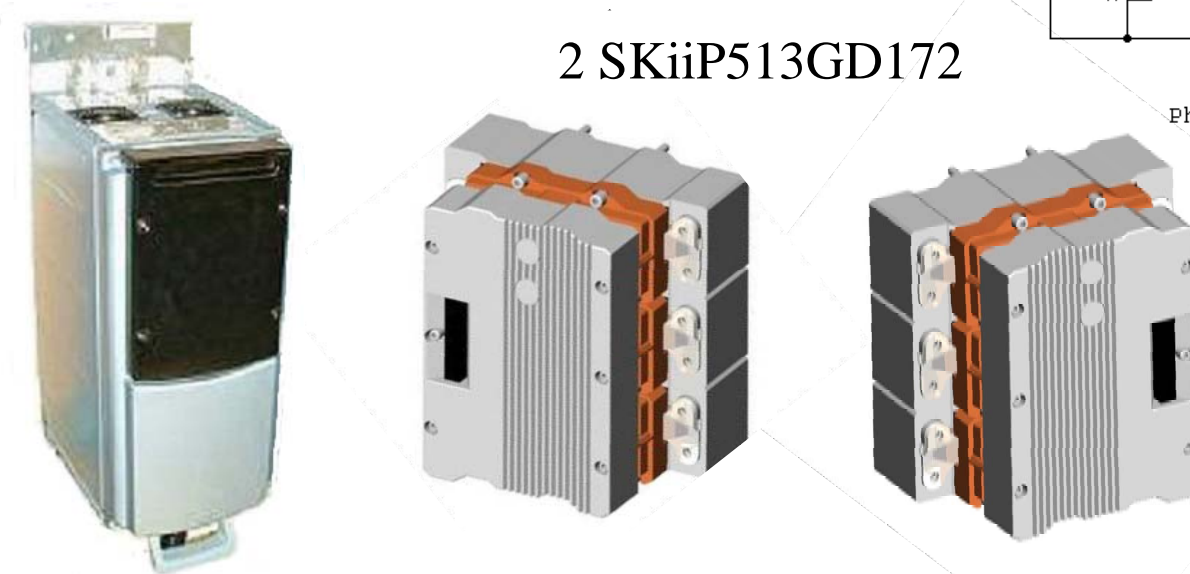


Compact power construction for 690V

Liquid cooling, DC link capacitors, drivers,
protection and PWM controller



2 SKiP513GD172



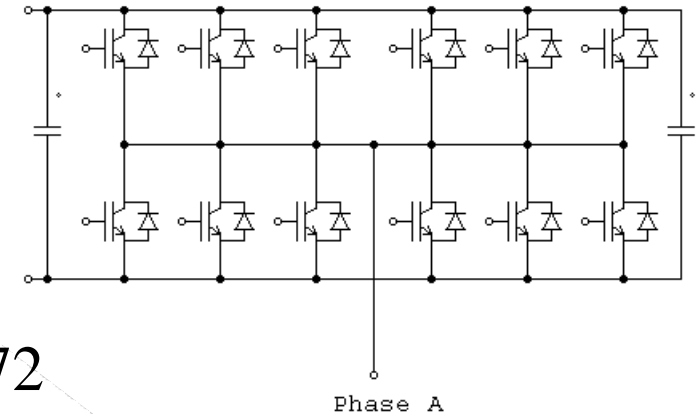
600kVA; Three-Phase Inverter; volume 50 liter, 12kVA / liter

Example with a 600kVA base unit



- High Power compact construction for 690V.
- Liquid cooling, DC link capacitors, drivers & protections, PWM controller

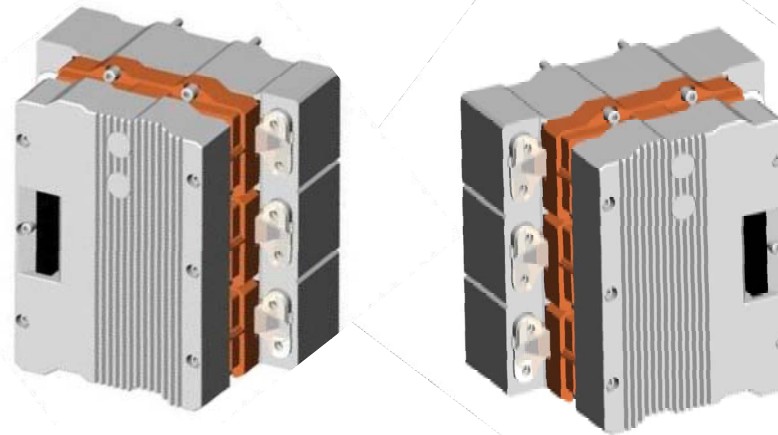
3 x



3 x 2//SKiiP1513GB172



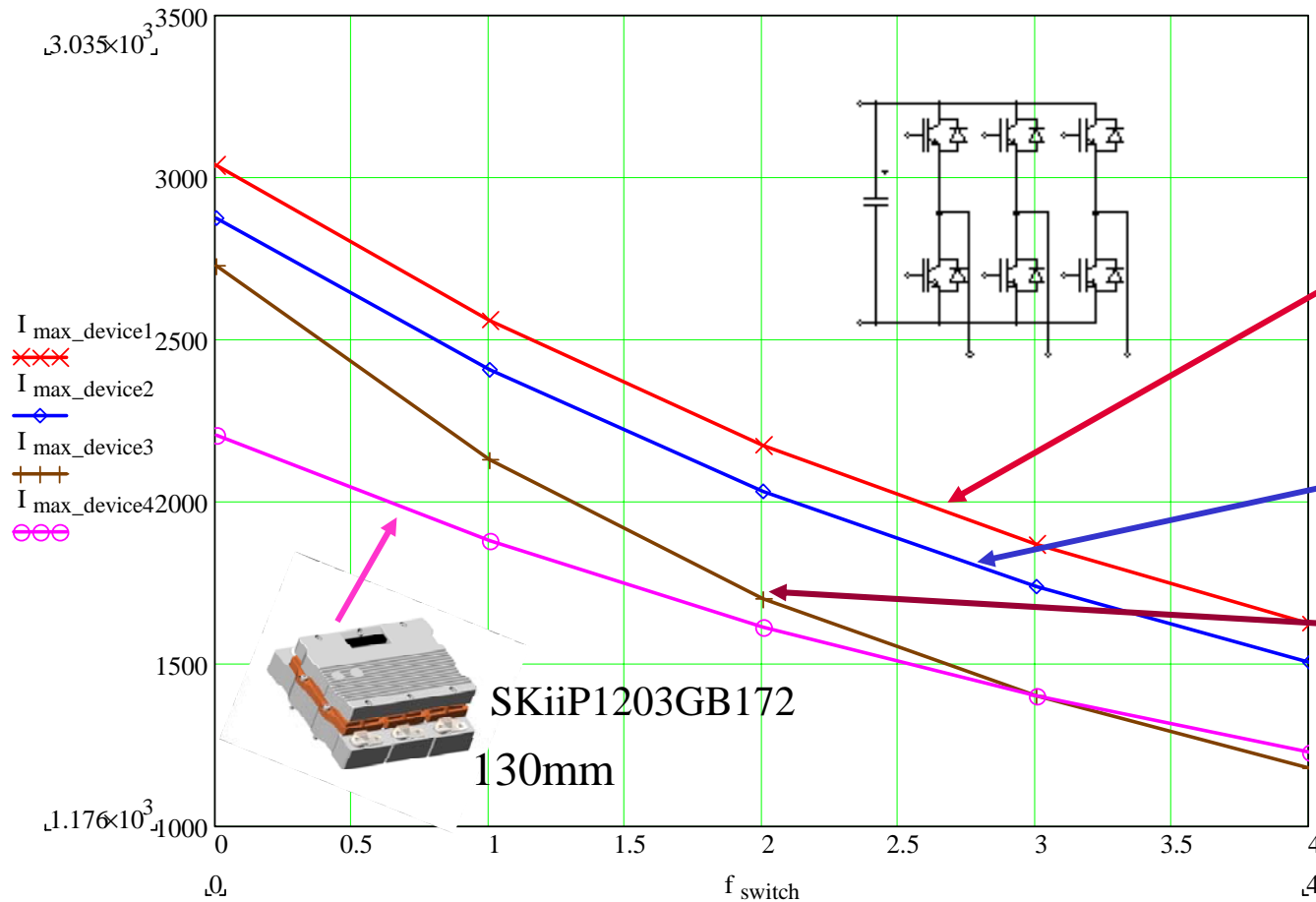
1800kVA



Example with 1800kVA base unit



1700V power semiconductors under same operation conditions



SKiiP1803GB172



SKiiP1513GB172



2 modules
2400A, 1700V



190mm

Load current vs. switching frequency



Solutions for parallel operation of the IGBT modules

1. One unit for the whole power

One driver and a lot of IGBT Modules in parallel. Each IGBT Module has its own gate resistors

2. Paralleling of Power STACKs

Two or more gate drivers are driving a group of IGBT modules. One PWM signal is connected in parallel to each driver.

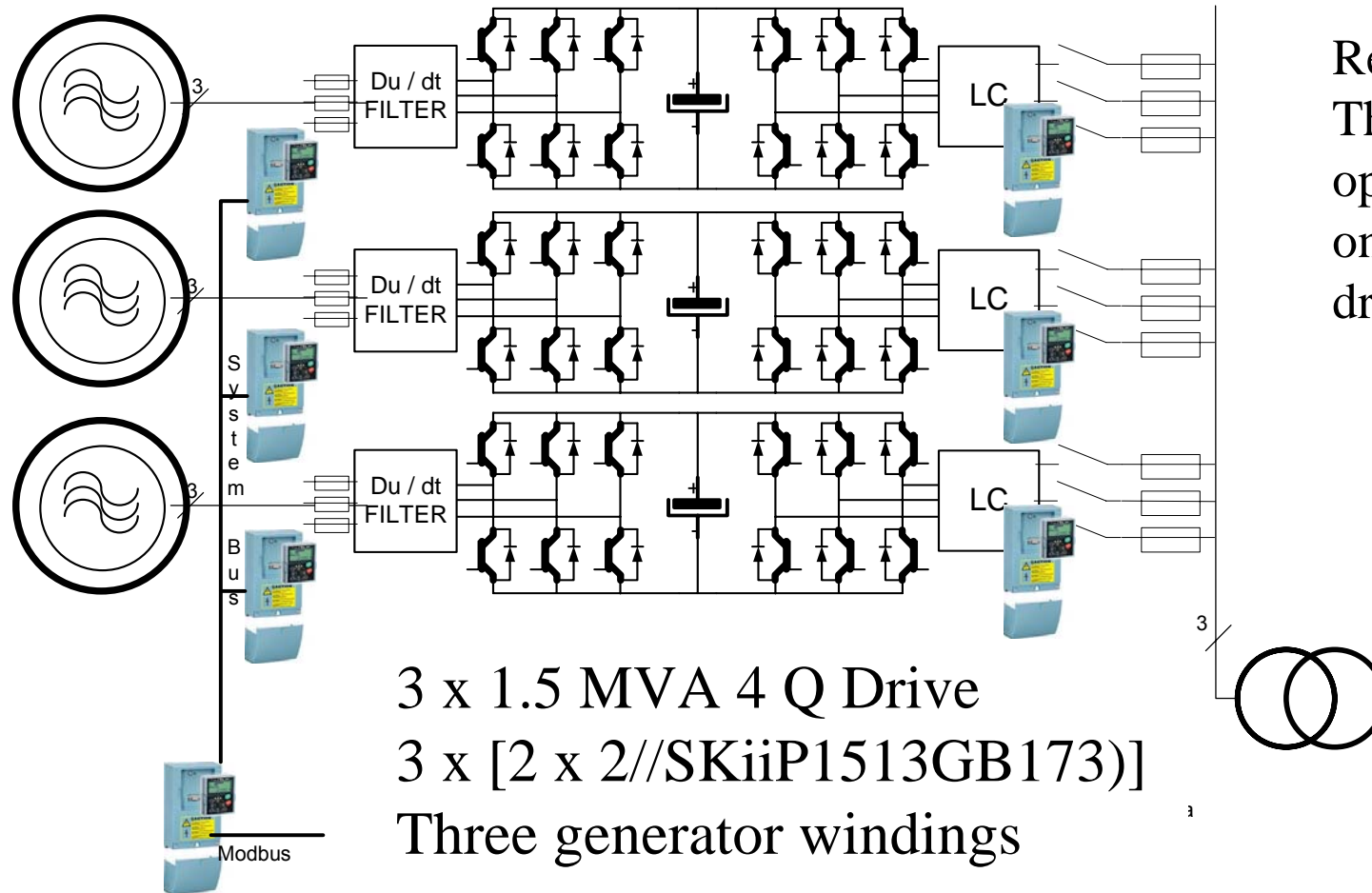
3. Controlled load current sharing of parallelized Power STACKs (Sophisticated PWM control)

4. Galvanic isolation on one side

(easy paralleling of standard independent basic units)

Paralleling of IGBT Modules

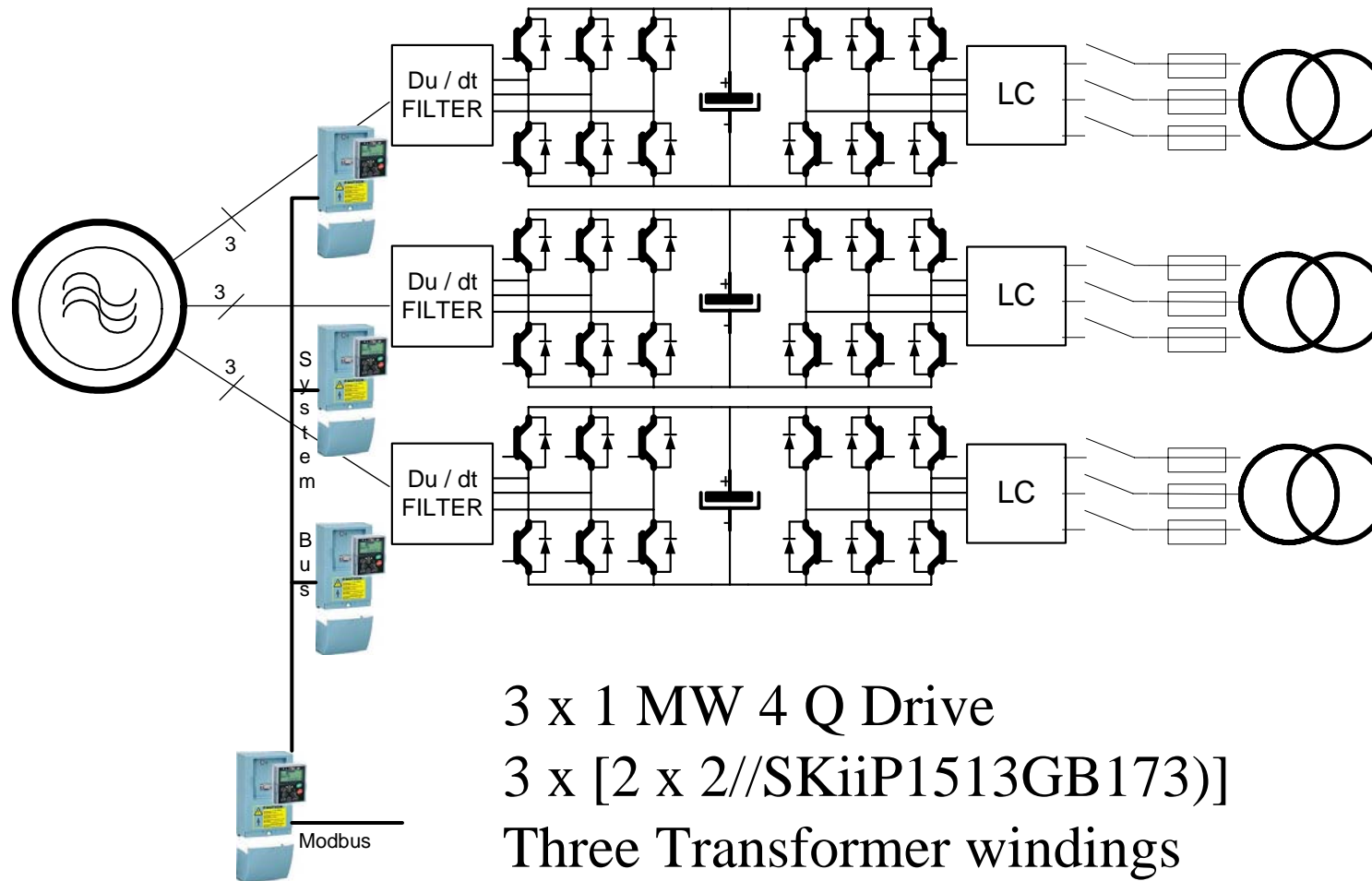




Redundancy:
The drive can
operate with
one or two
drives in parallel

**Three independent 4Q drives in parallel, with
separate motor windings**





Redundancy:
The drive can
operate with
one or two
drives in parallel

Three independent 4Q drives in parallel, with separate transformer windings





1.5 MVA, 4 Q drive cabinet

- Medium Voltage Levels:
 - 2.3 kV, 3.3 kV, 4.16 kV, 6.3 kV, 11 kV, 13.8 kV.....35kV

- Motor Power Range: 200kW ... 6000 kW 11MW.....50MW
- Semiconductor Blocking Voltage Range:
 - 1.2 kV, 1.7 kV, 2.5kV, 3.3kV, 4.5 kV , 6.5kV

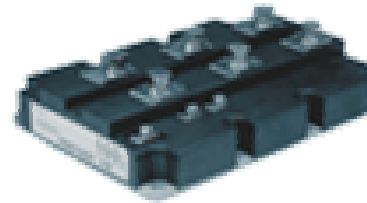
- Line / (Semiconductor Voltage Range):
 - 480Vac/ (1200V); 690Vac/(1700V), 1250Vdc/(2500V),
 - 1800Vdc / (3.3kV); 2.2kVdc / (4.5kV); 3.3 kVdc/ (6.5kV)

Medium Voltage Values & Semiconductors



■ MV voltage source inverter

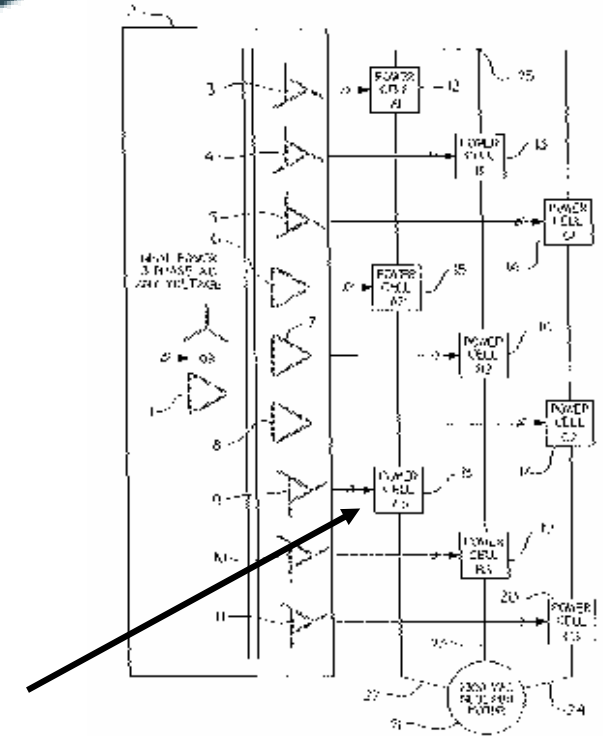
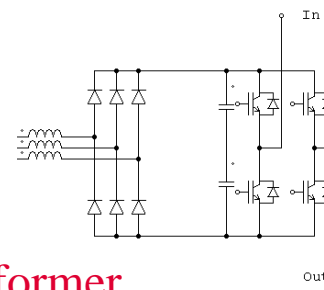
- ◆ 3.3kV 4.5kV and 6.5 kV IGBT semiconductors, for Three Level Inverter for 3.3kV, 4.2kV and 6.3kV Medium Voltage lines



◆ IGCT based inverters



- ◆ Cell MV construction with low voltage silicon. (1700V)



All MV Drive solutions have a full size input transformer

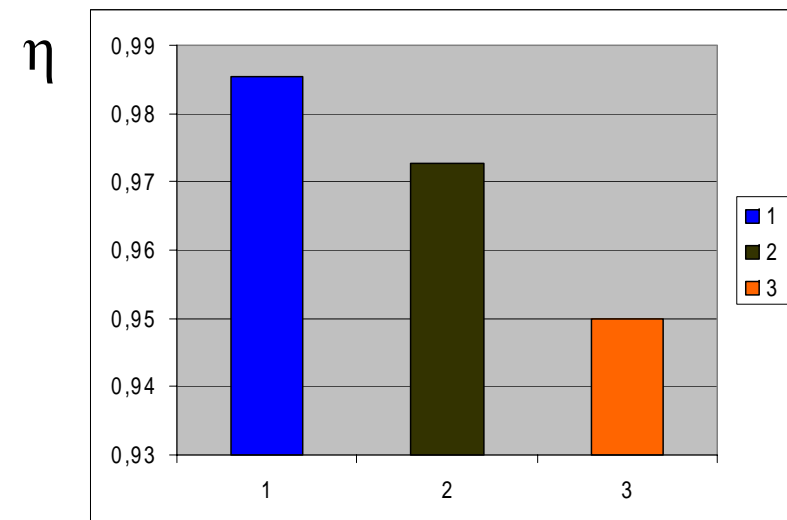
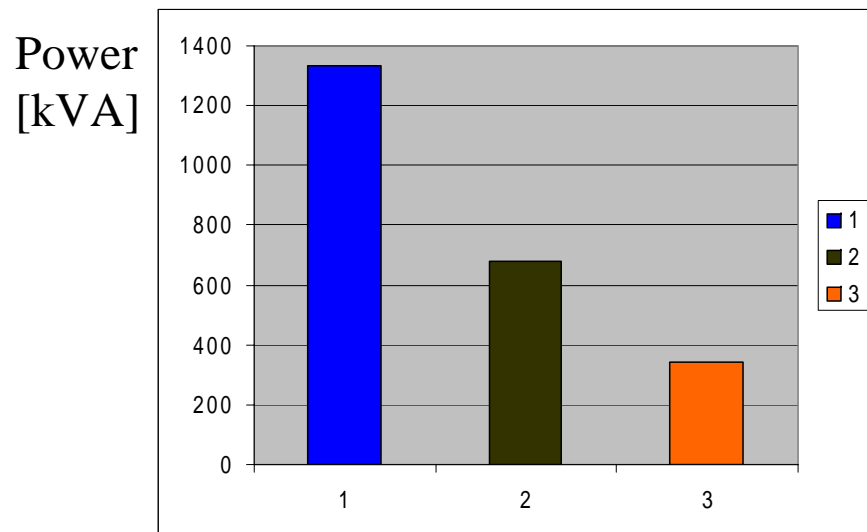
Existing solutions of MV drives



Three phase IGBT inverter operation at same cooling conditions and
Fsw= 3.6kHz; cosφ=0.9 and same module size



1.7kV, 2400A	3.3kV, 1200A	6.5kV, 600A
Vdc=1100V	Vdc=1800V	Vdc=3600V
Vac=690V	Vac=1130V	Vac=2260V



**Efficiency comparison of
different blocking voltage IGBTs**



Windmill designers Goals

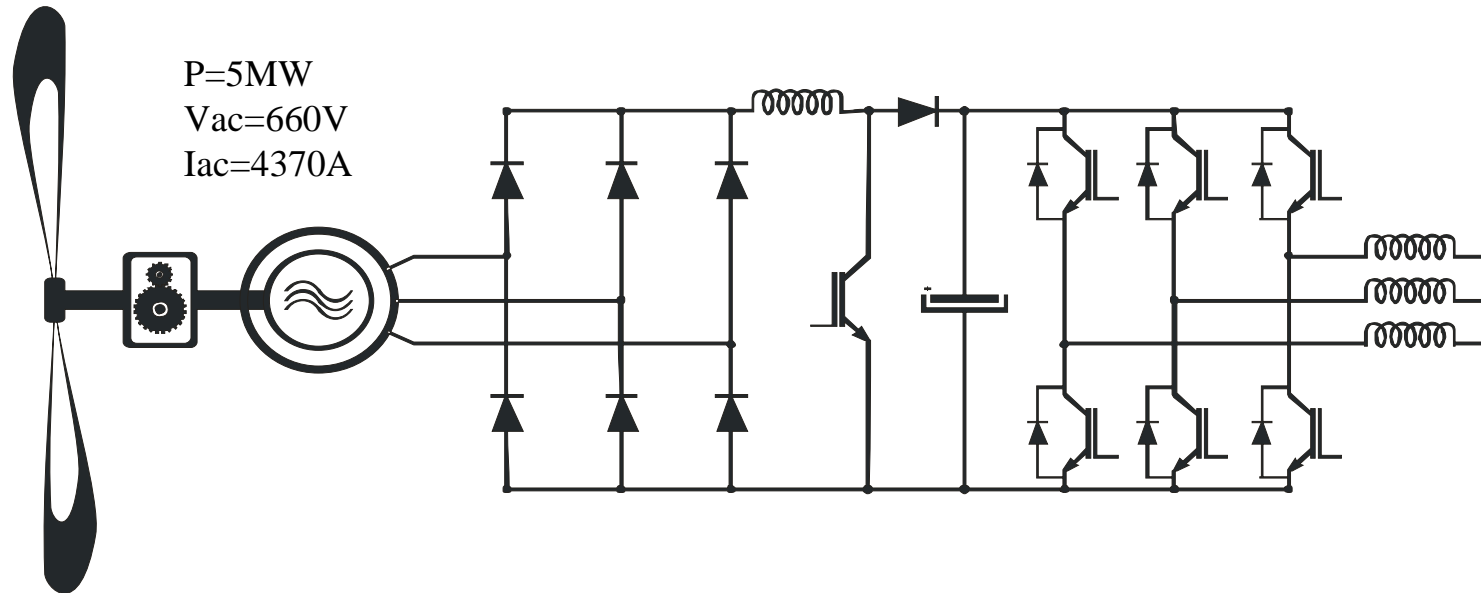
- High Power Wind turbine
- Lower losses
- Result: Medium Voltage Motor - Generator
- Variable speed
- High efficiency
- Proven semiconductors
- Clean, sinusoidal line current with simple line transformer
- Good line power factor, and low THD
- Active and Reactive power control
- Modular construction for different voltages, powers for quick assembly
- High reliability
- Lowest costs

Goals for Variable Speed Wind Turbines



Proven construction

Low voltage 5 MW Variable Speed Wind Turbines With Synchronous Motor / Generator



Synchronous motor / generator with the rectifier, boost chopper, and line-side converter for the full generated power

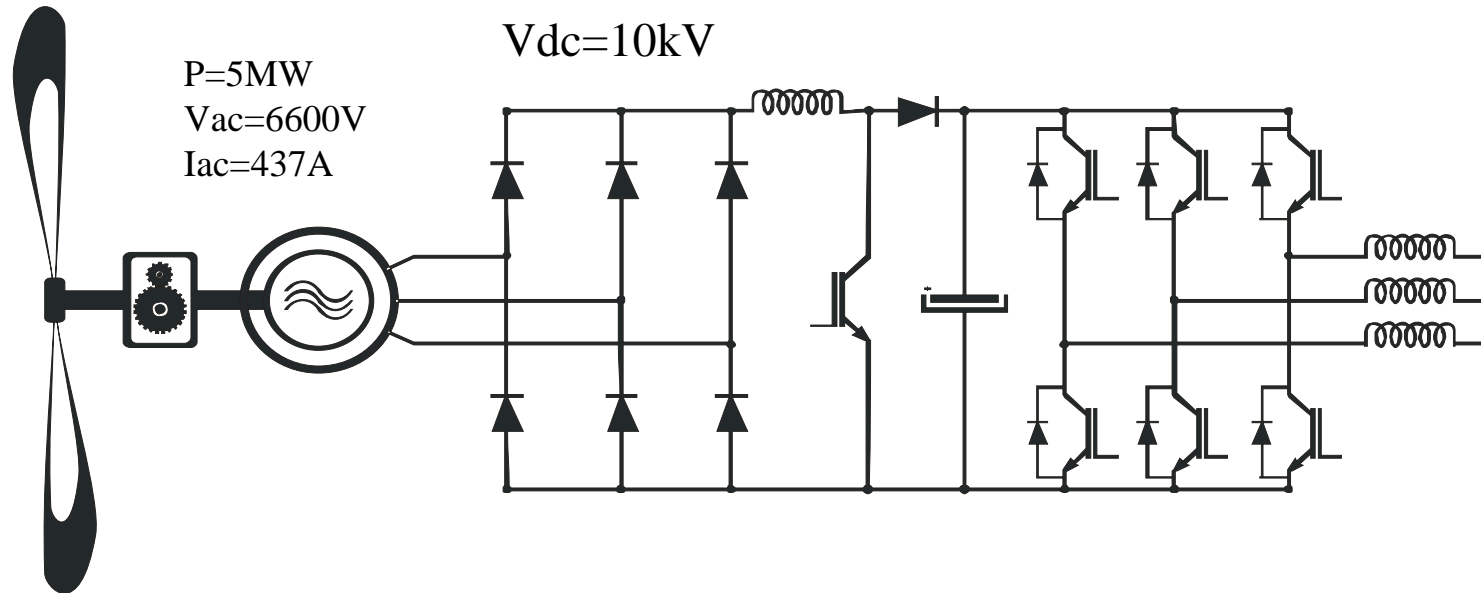
Well known construction with up to 15 units in parallel.
Total number of running units > 20.000

Low voltage Variable Speed Wind Turbines



Can we make the equivalent MV construction ?

**5 MW Variable Speed Wind Turbines
With Synchronous Motor / Generator**



Synchronous motor / generator with the rectifier, boost chopper, and line-side converter for the full generated power

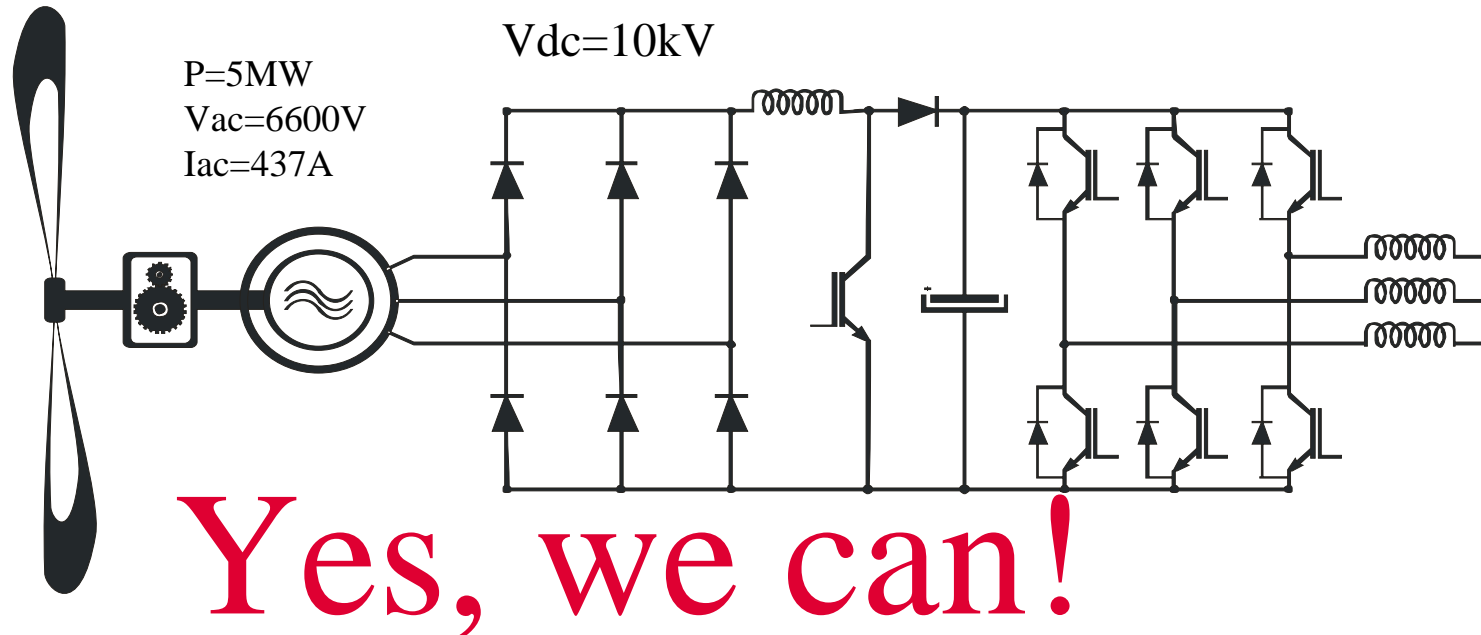
$V_{dc}=10\text{ kV}$; There is no semiconductors for a such high DC voltage!

Medium Voltage Variable Speed Wind Turbine



Can we make the equivalent MV construction ?

**5 MW Variable Speed Wind Turbines
With Synchronous Motor / Generator**

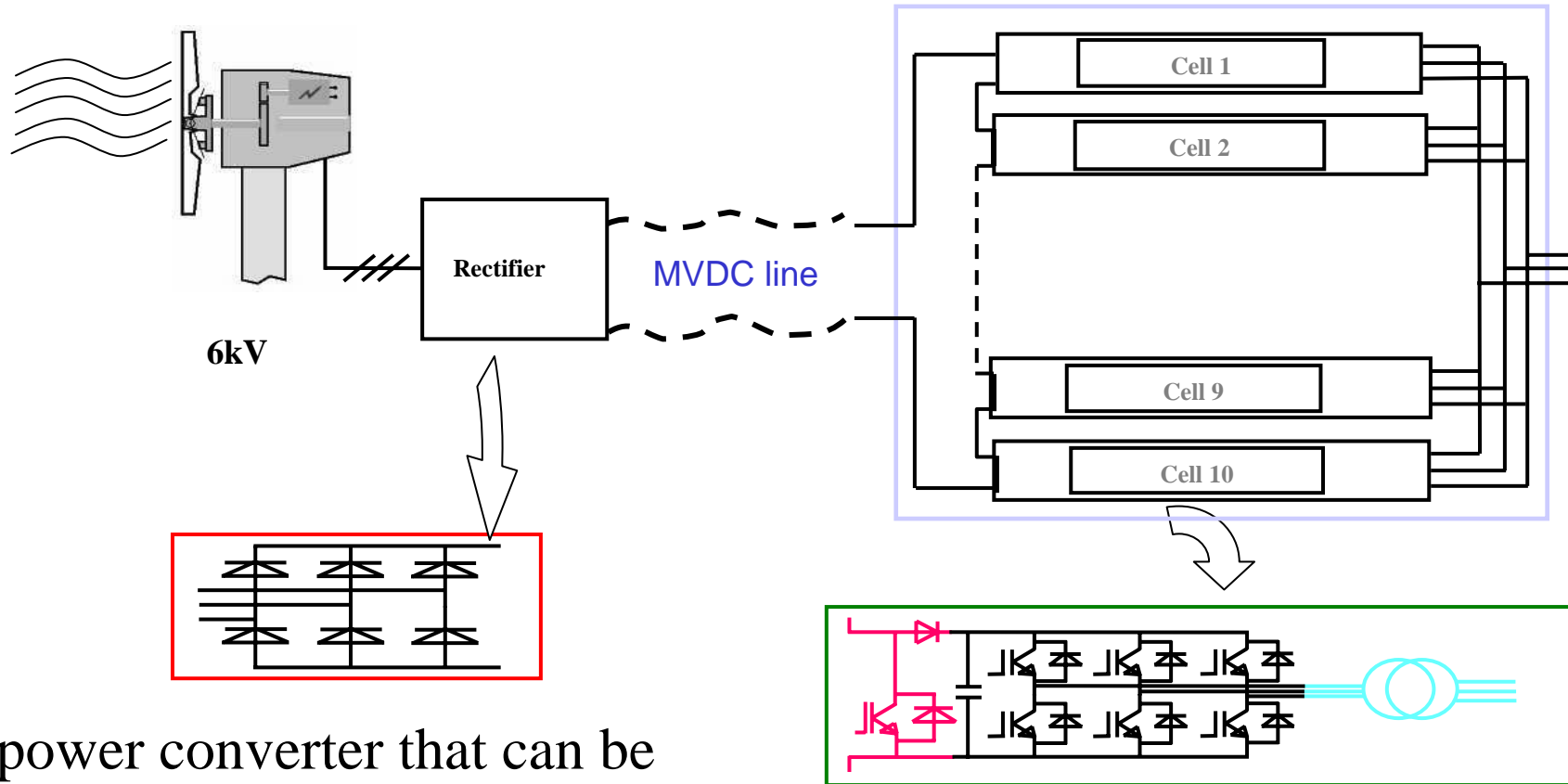


Synchronous motor / generator with the rectifier, boost chopper, and line-side converter for the full generated power

$V_{dc}=10\text{ kV}$; There is no semiconductors for a such high DC voltage!

Medium Voltage Variable Speed Wind Turbine



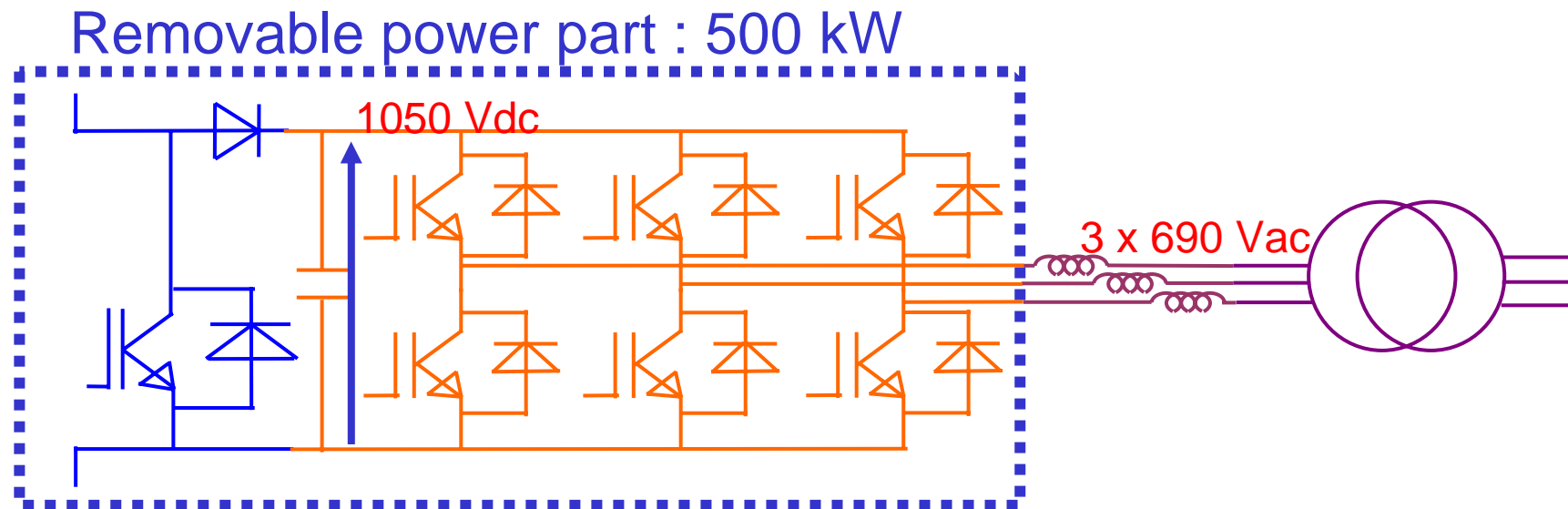


A power converter that can be placed on the bottom of the tower (less weight in the nacelle),

SEMIKRON MV Cell

Medium Voltage Windmill on Cell Principle

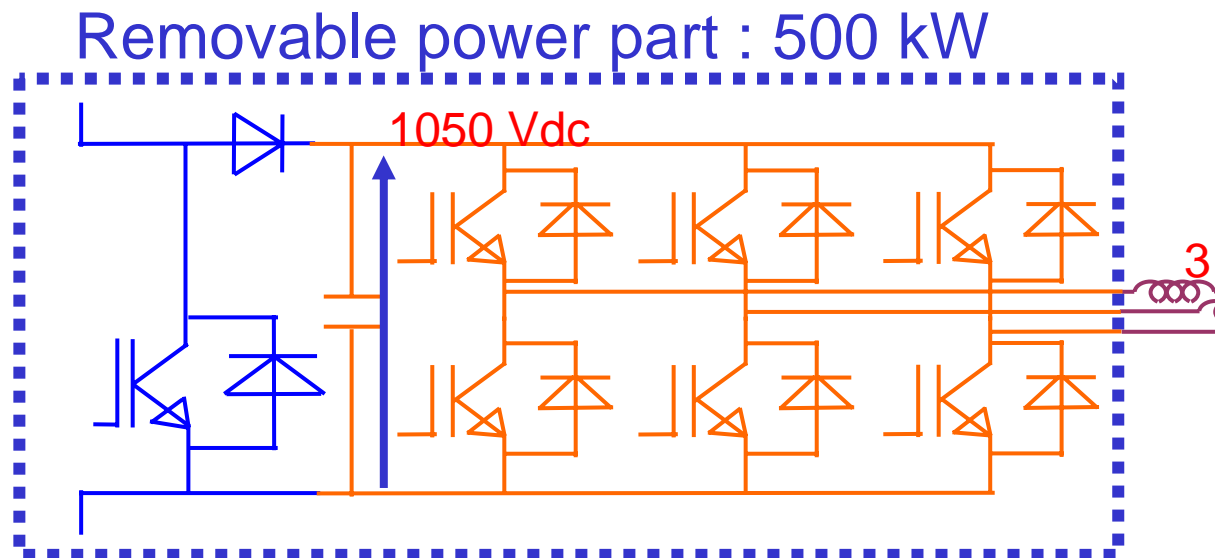
Only LOW VOLTAGE SEMICONDUCTORS



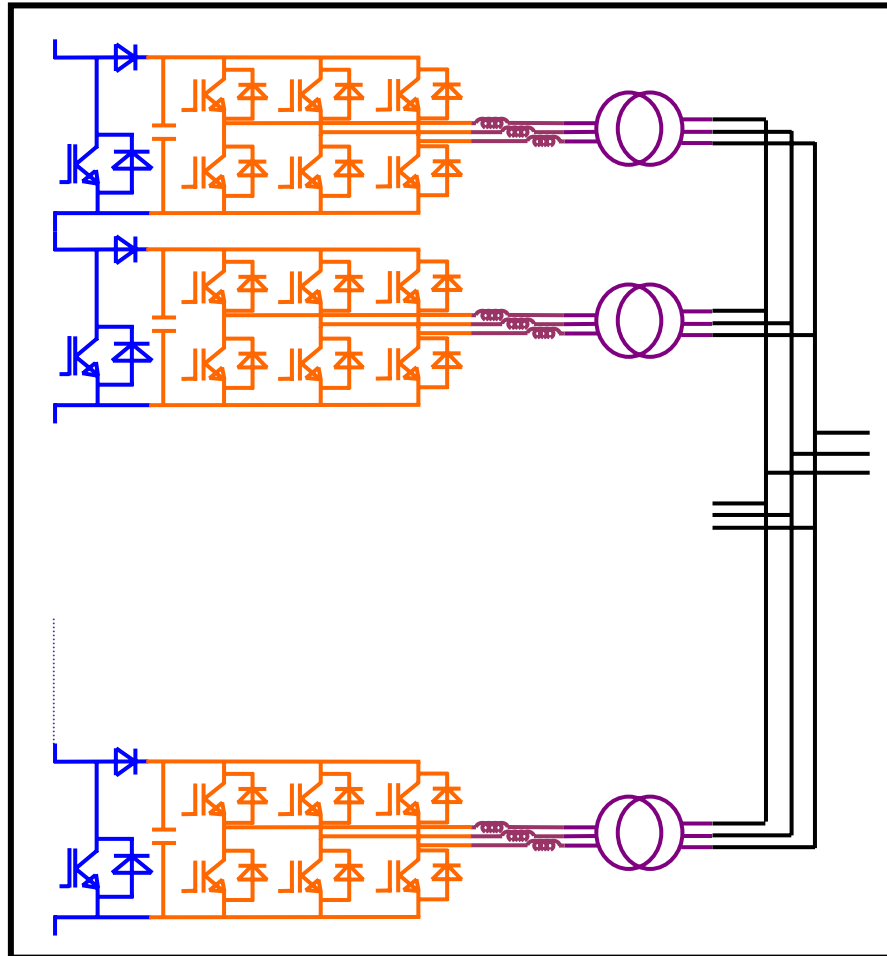
Basic 600 kVA, 500kW cell



Only LOW VOLTAGE SEMICONDUCTORS



Basic 600 kVA, 500kW cell

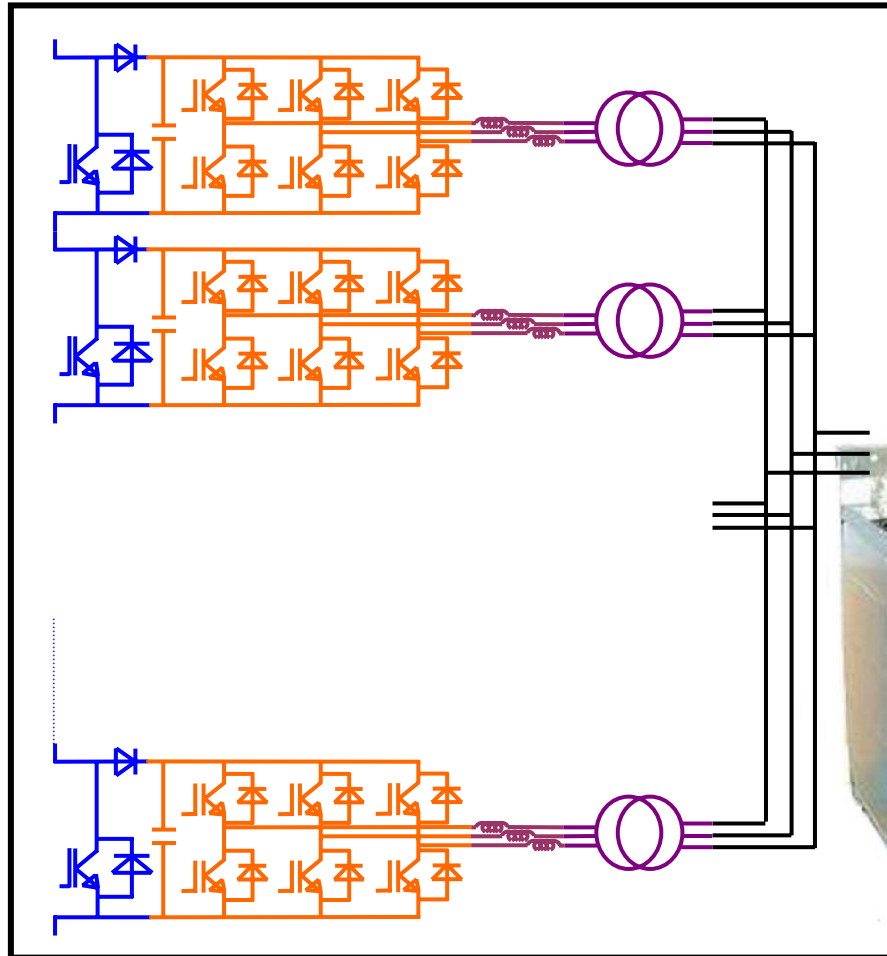


MODULARITY

- Series connections of Cells for different voltages
- Parallel connections in one Cell for various power ranges

Complete inverter construction





MODULARITY

- Series connections of Cells for different voltages
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Complete inverter construction

Variable Speed Wind Turbines With Medium Voltage AC Synchronous Motor

Features

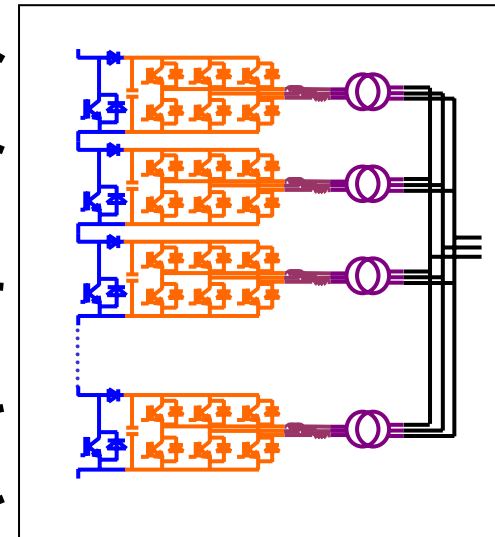
- Generator DC voltage range from 0V to $V_{dc_{max}}$
- DC voltage per cell 1000V(1700V silicon)
- Vdc Max per Cell 1200V
- Number of Cells = $V_{dc_{max}}/V_{cell} (+1)$
- Cell Power: $P_{gen_{max}}/Number\ of\ Cells$
- Redundancy of the system (+1)
- Cell switched-on time varies from 0% to 100%
- Switched-off Cell can produce full reactive power
- High efficiency at lower power
- Line side ripple frequency = $N_{cell} * F_{sw_{cell}}$
- Simple line side transformer

Solution for Variable Speed Wind Turbines



All Power Electronics installation
is in only one container

MVDC connection

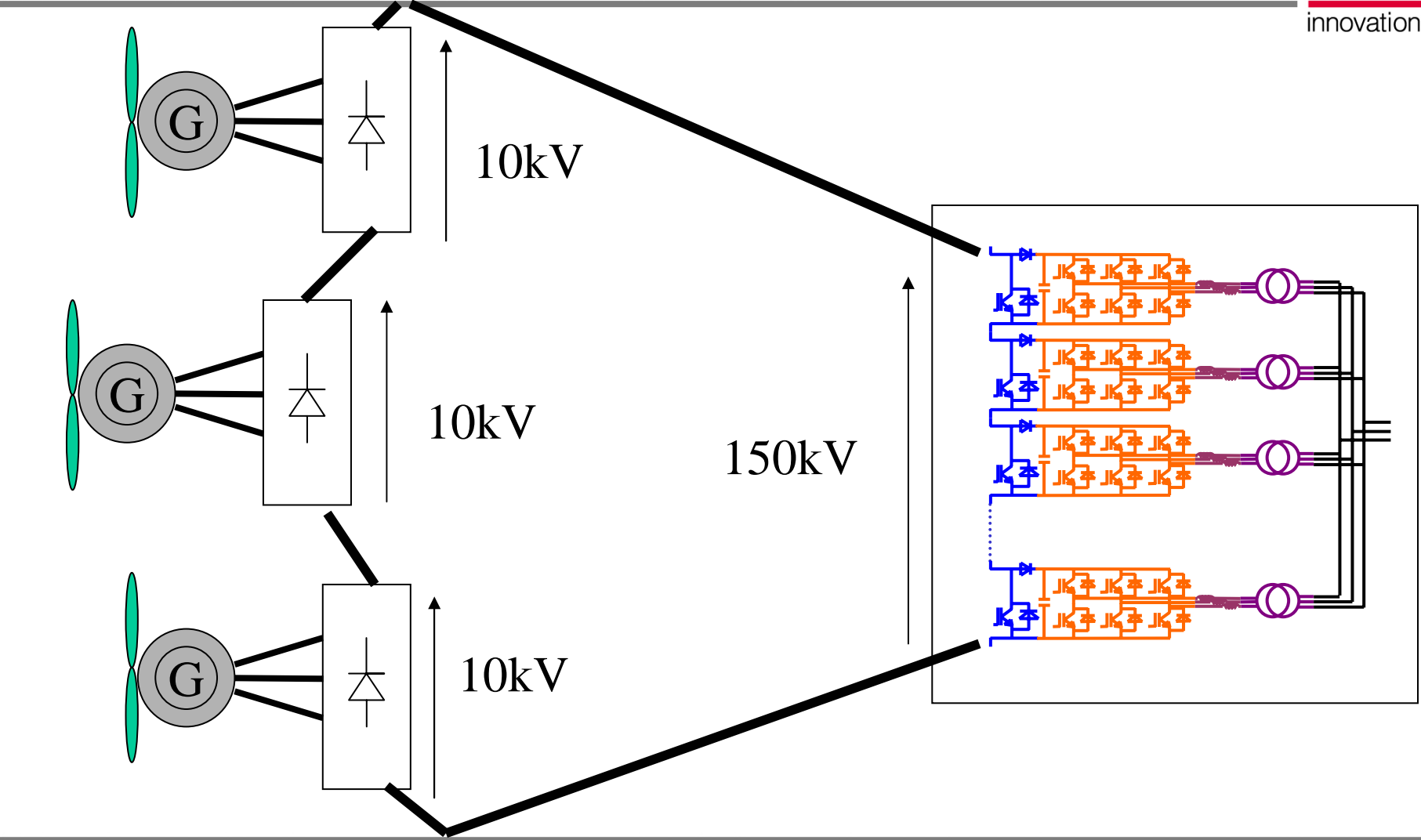


Efficient power distribution can
be achieved at the distances
with 1kVdc per 1km

Wind park concept



Connecting several windmills in series for DC voltages of 100kV or more; the power converter is on the shore, and the windmills are connected with a single cable



Series connection of several windmills

STATCOM Static Compensator:
allows both leading or lagging
power factor; voltage
stabilization and load
balancing

Active Filter and STATCOM
for unlimited power range



2 MVA
& 690V

High Voltage

